

Lecture 2, slide 2:

$$V_{ab} = -1V$$

$$V_{ca} = -2V$$

$$V_{cb} = V_{ca} + V_{ab} = -3V$$

slide 26:

Σ current leaving - Σ currents entering = 0

$$10mA + i + 15mA - 5mA = 0$$

$$i = -20mA$$

slide 28:

using generalized KCL, $-i + 5\mu A + 2\mu A = 0$

$$i = 7\mu A$$

slide 33:

$$\text{Path 1: } -V_a + V_2 + V_b = 0$$

$$\text{Path 2: } -V_b - V_3 + V_c = 0$$

$$\text{Path 3: } -V_a + V_2 - V_3 + V_c = 0$$

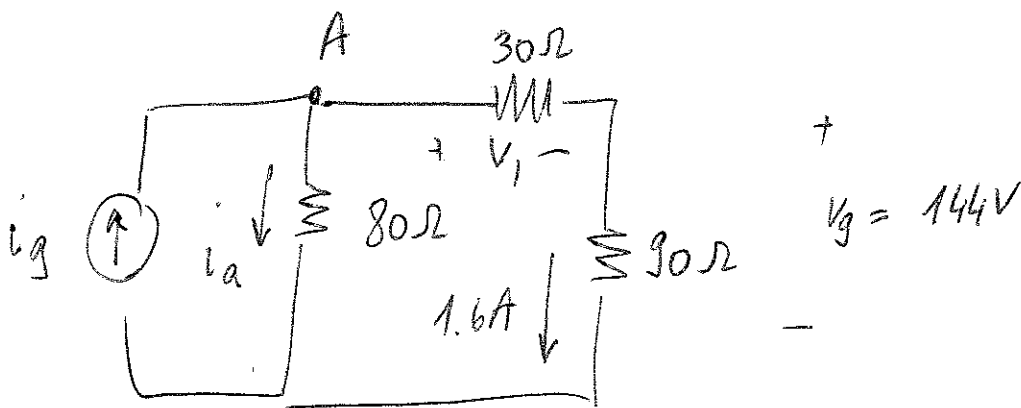
slide 39 :

$$V_2 = \frac{R_2}{R_1 + R_2 + [(R_3 + R_4) \parallel R_5]} \cdot V_{SS}$$

$$\neq \frac{R_2}{R_1 + R_2 + R_3 + R_4} \cdot V_{SS}$$

slide 43 :

$$V_g = 90\Omega \cdot 1.6A = 144V$$



$$V_1 = 1.6A \cdot 30\Omega = 48V$$

$$\Rightarrow V_A = V_1 + V_g = 48V + 144V = 212V$$

$$i_a = \frac{V_A}{R_{80\Omega}} = \frac{212}{80} A$$

Lecture 3 Slide 3:

$$i_2 = 0$$

$$V_{\Delta} = \frac{5k}{5k+1k} \cdot 60V$$

$$= 50V \quad (\text{Voltage division})$$

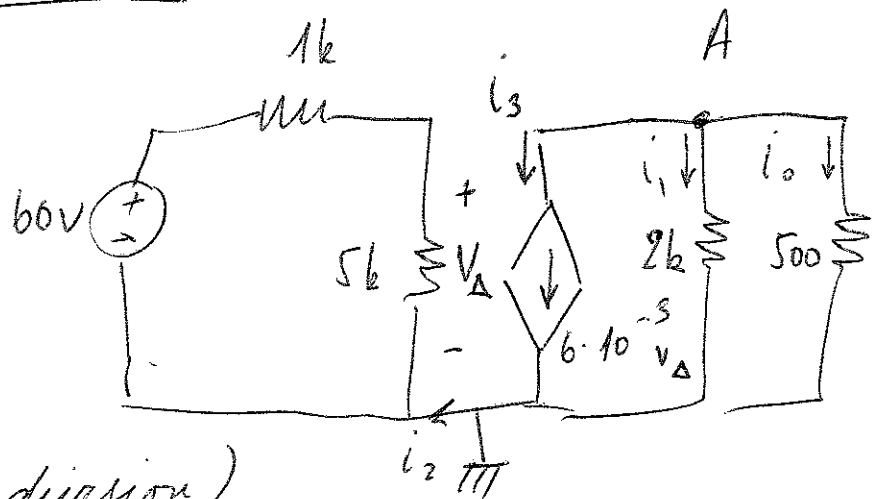
$$i_3 = 50V \cdot 6 \cdot 10^{-3} = 0.3A$$

$$2k\Omega \parallel 500\Omega = 400\Omega$$

$$\Rightarrow V_A = -i_3 \cdot 400\Omega = 12V$$

$$i_1 = \frac{12V}{2k} = 0.06A$$

$$i_0 = \frac{12V}{500} = 0.24A$$

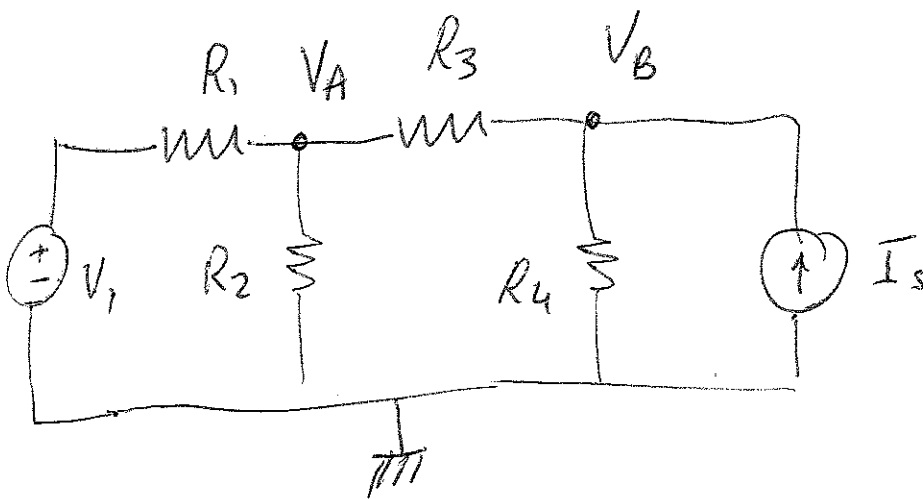


Slide 5:

$$R_{eq} = [(R_1 + R_2) \parallel R_3] + [(R_4 + R_5) \parallel R_6]$$
$$= 8k\Omega$$

$$I = \frac{7V}{8k\Omega}$$

Slide 7:

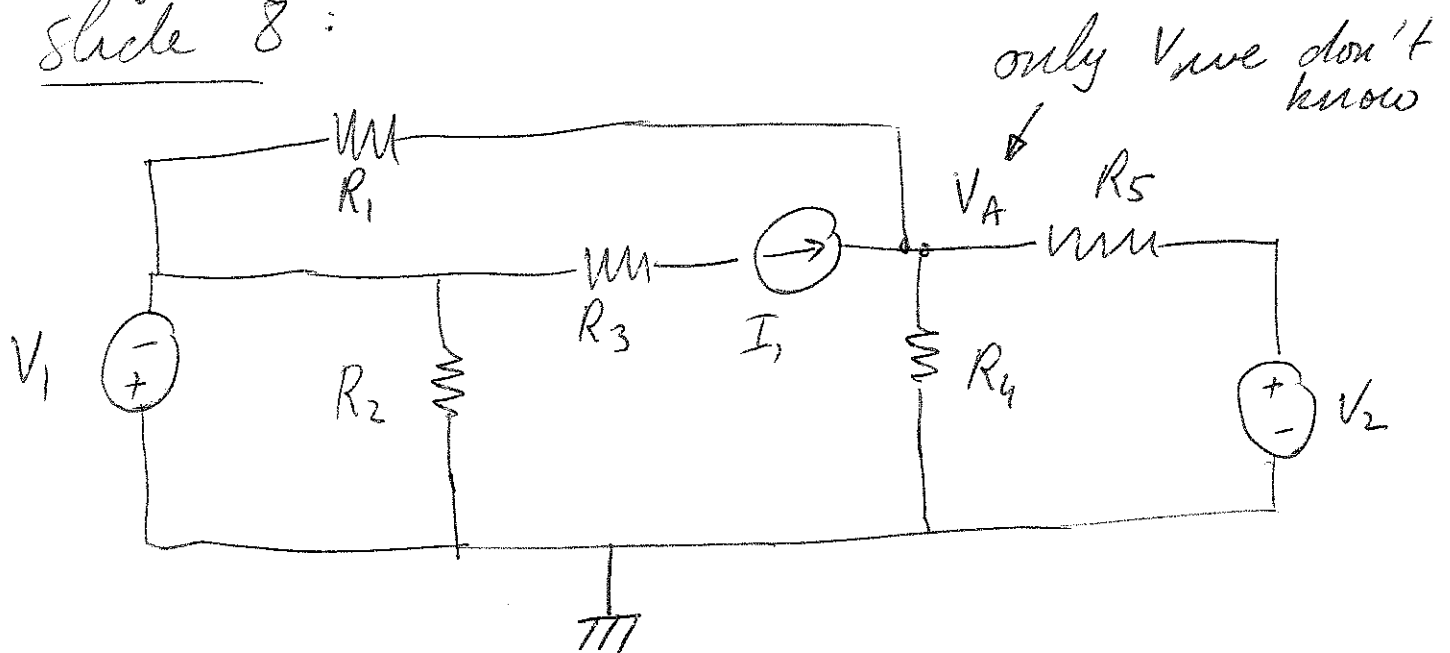


$$\text{KCL @ } V_A: \frac{V_A - V_1}{R_1} + \frac{V_A}{R_2} + \frac{V_A - V_B}{R_3} = 0$$

$$\text{KCL @ } V_B: \frac{V_B - V_A}{R_3} + \frac{V_B}{R_4} + (-I_s) = 0$$

\rightarrow 2 eq. 2 unknown.

slide 8:

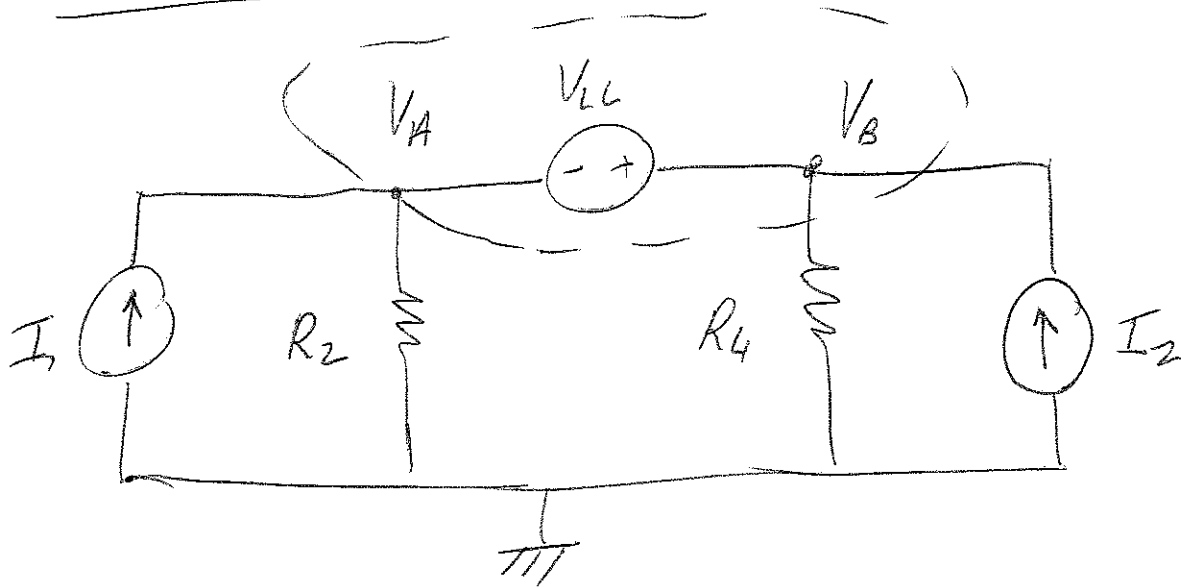


KCL @ V_A :

$$\frac{V_A + V_1}{R_1} + \frac{V_A}{R_4} + \frac{V_A - V_2}{R_5} + (-I_1) = 0A$$

one equation, one unknown.

Slide 11:

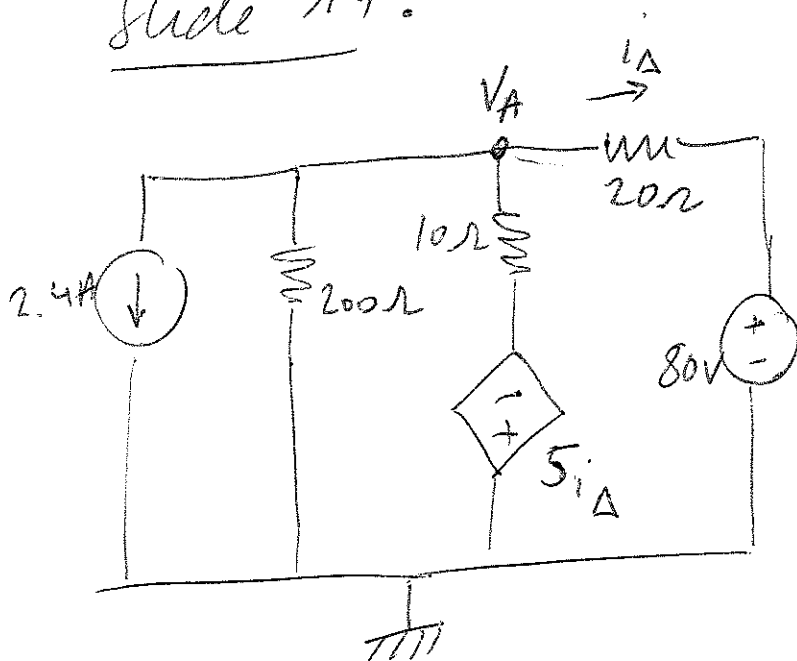


KCL @ supernode:

$$\begin{cases} -I_1 + \frac{V_A}{R_2} + \frac{V_B}{R_4} - I_2 = 0 \\ V_B = V_A + V_{LL} \end{cases}$$

2 eq.,
2 unknown

Slide 14:

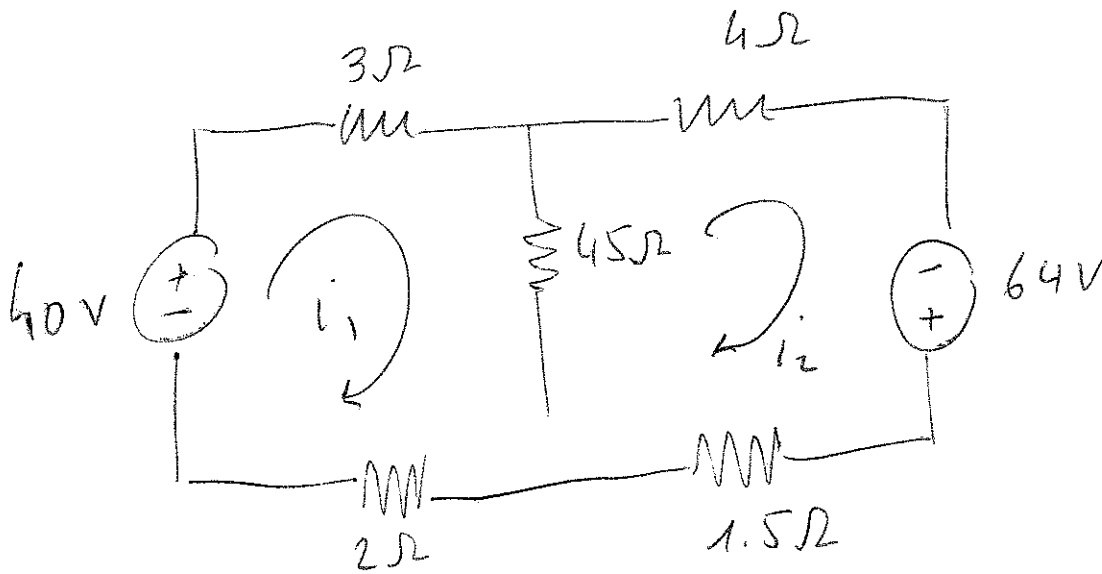


KCL @ VA

$$\begin{cases} 2.4A + \frac{V_A}{200} + \frac{V_A - 80}{20} + \frac{V_A - (-5i_{\Delta})}{10} = 0 \\ i_{\Delta} = \frac{V_A - 80}{20} \end{cases}$$

2 equations
2 unknown

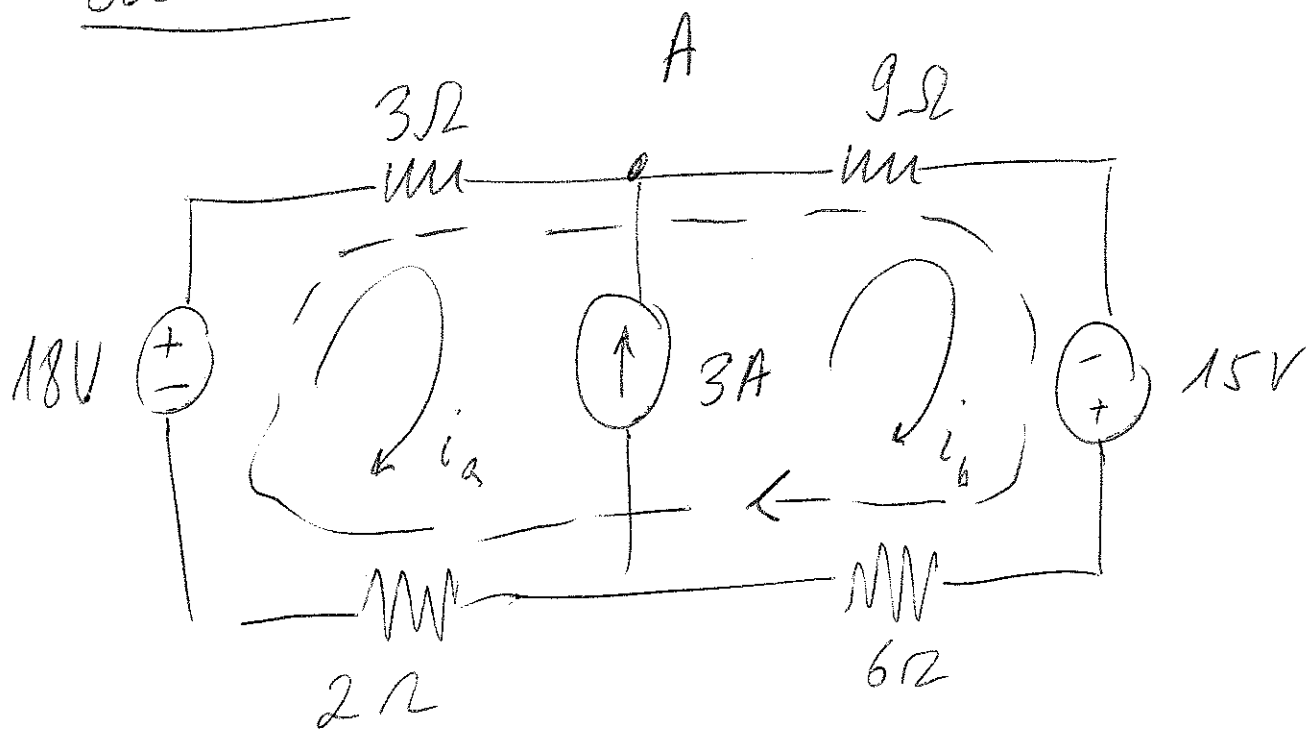
slide 16



$$\left. \begin{array}{l} 2_{eq} \\ 2_{uk} \end{array} \right\} \begin{array}{l} \text{KVL @ } i_1 : \\ -40V + i_1 \cdot 3\Omega + (i_1 - i_2) 45\Omega + i_1 \cdot 2 = 0V \\ \text{KVL @ } i_2 : \\ -64V + i_2 \cdot 1.5\Omega + (i_2 - i_1) 45\Omega + i_2 \cdot 4\Omega = 0 \end{array}$$

$uk = \text{unknown}$

Slide 18:



KVL @ supermesh:

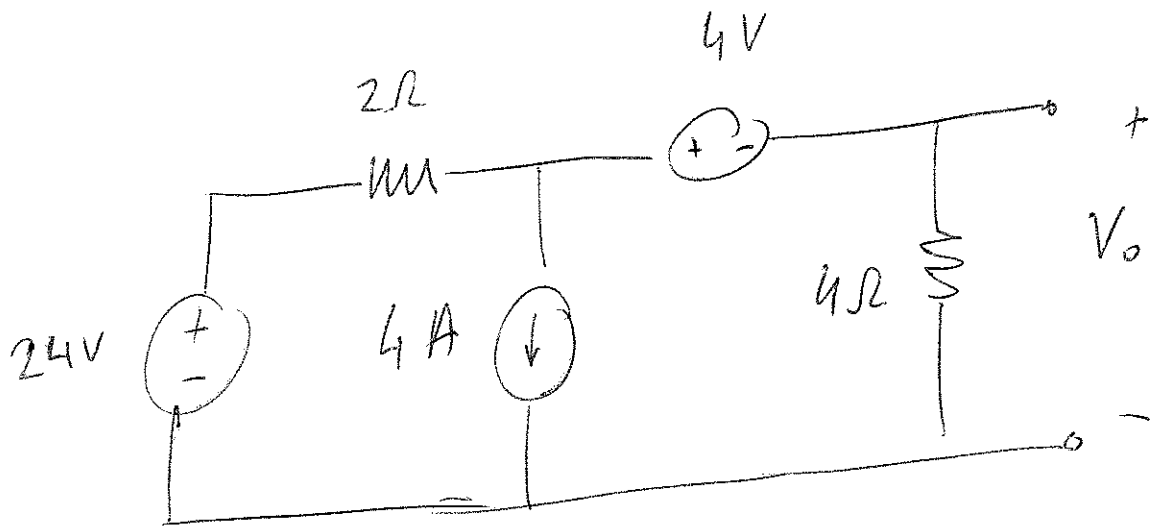
$$-18V + i_a \cdot 3\Omega + i_b \cdot 9\Omega - 15V + i_b \cdot 6\Omega + i_a \cdot 2\Omega = 0V$$

also, KCL @ A:

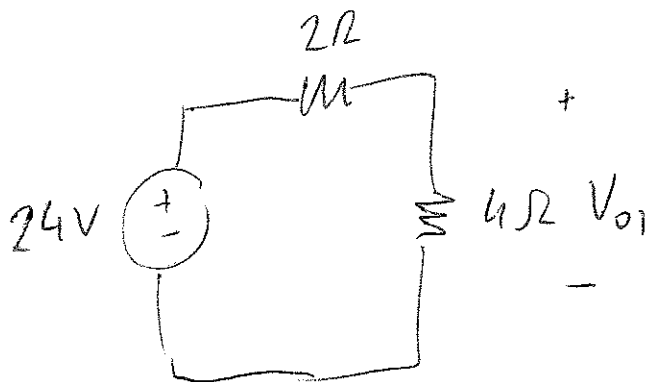
$$-i_a - 3A + i_b = 0$$

uk = unknown

Slide 23:

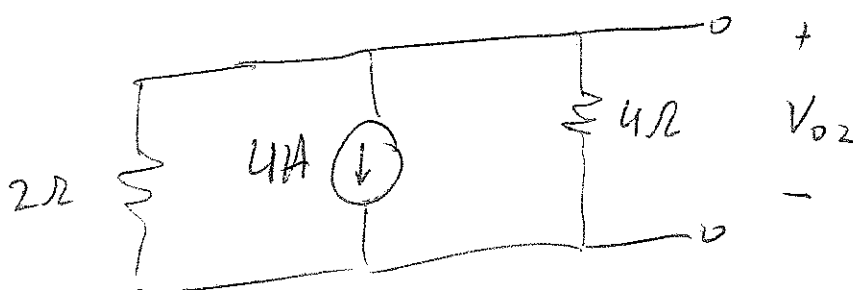


Contribution from 24V source. Turn all other sources off:



$$V_{o1} = \frac{4}{2+4} \cdot 24V = 16V$$

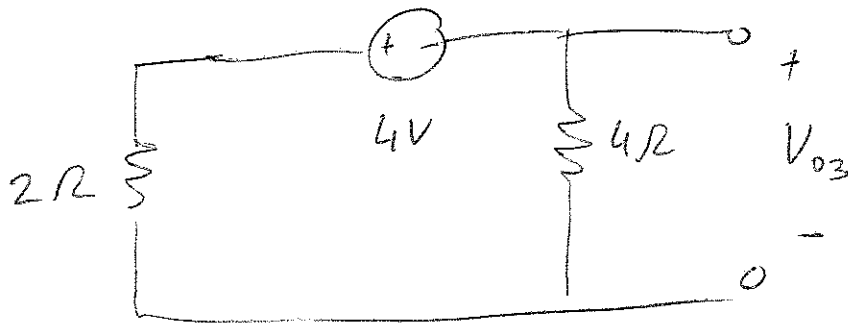
Contribution from 4A source:



$$\begin{aligned} R_{eq} &= \left(\frac{1}{2} + \frac{1}{4} \right)^{-1} \\ &= \frac{4}{3} \Omega \\ \Rightarrow V_{o2} &= -4A \cdot R_{eq} \\ &= -\frac{16}{3} V \end{aligned}$$

(... cont'd)

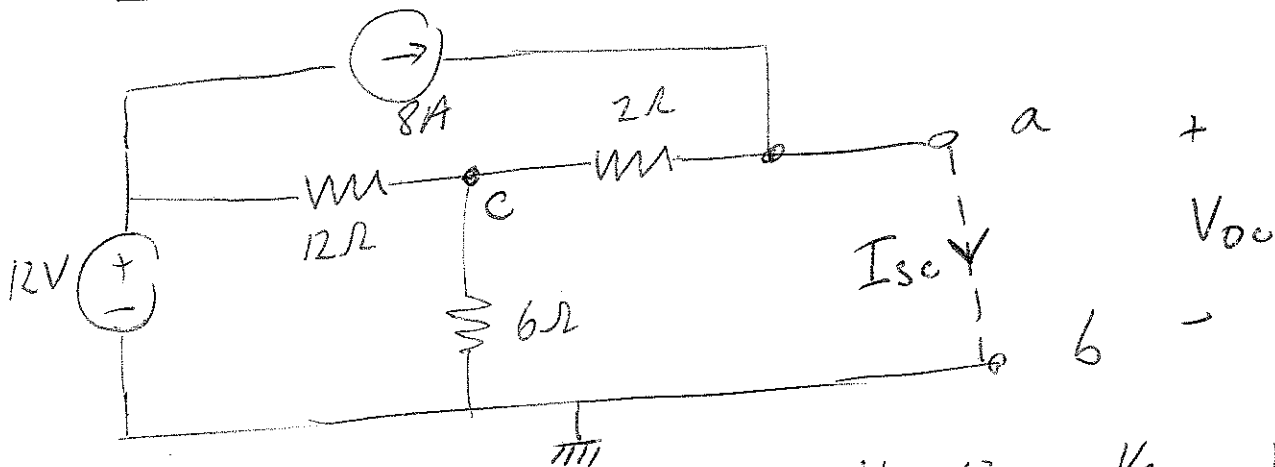
Contribution from 4V source:



$$V_{o3} = -4V \cdot \frac{4\Omega}{6\Omega} = -\frac{8}{3} V$$

$$V_o = \sum V_{oi} = 16V - \frac{16}{3}V - \frac{8}{3}V = 8V$$

Slide 30:



$$V_{Th} = V_{oc}: \text{KCL @ c: } \frac{V_c - 12}{12} + \frac{V_c}{6} + \frac{V_c - V_a}{2} = 0$$

$$\text{KCL @ a: } -8A + \frac{V_a - V_c}{2} = 0$$

→ solve for V_a

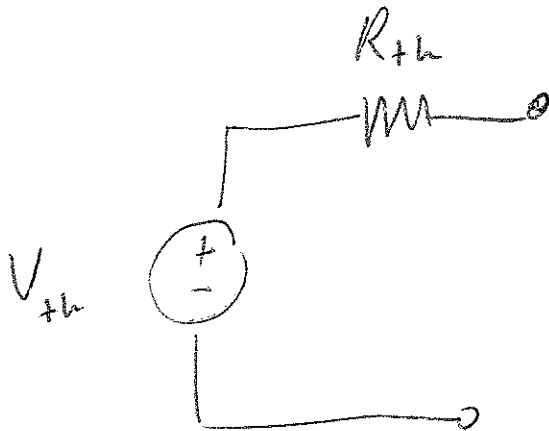
$$V_{Th} = V_a$$

$$R_{th} = \frac{V_{oc}}{I_{sc}}$$

I_{sc} : KCL @ C:

$$\frac{V_c - 12}{12} + \frac{V_c}{6} + \frac{V_c}{2} = 0 \quad \text{solve for } V_c$$

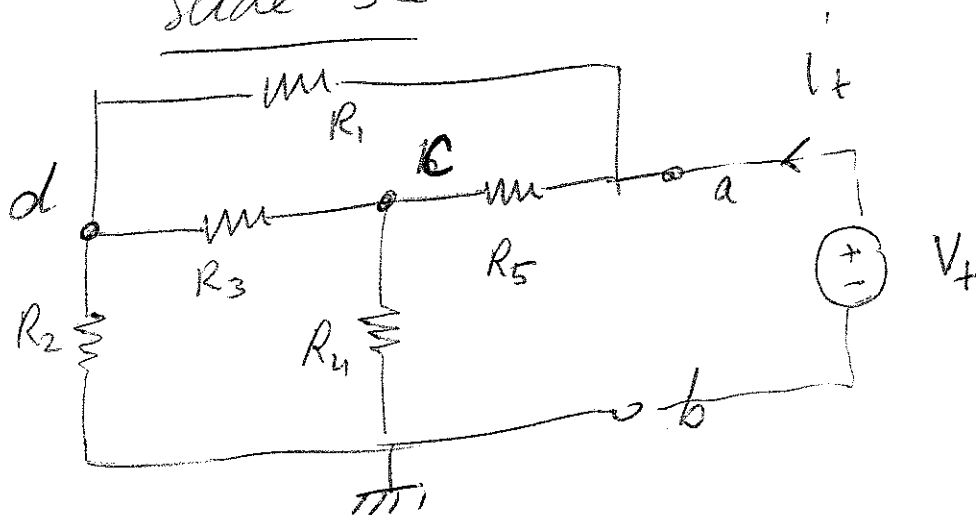
$$I_{sc} = 8A + \frac{V_c}{2\Omega} \quad [KCL @ a]$$



$$V_{th} = V_{oc}$$

$$R_{th} = \frac{V_{oc}}{I_{sc}}$$

Slide 32:



solve for
 V_t & i_t

(...)

(000)

KCL @ c:

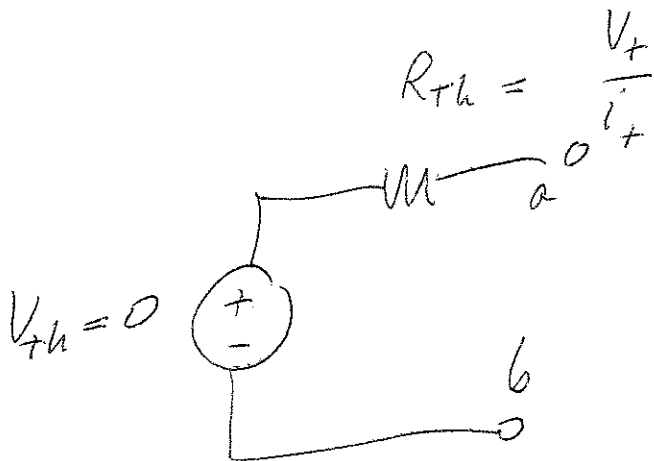
$$\frac{V_c - V_d}{R_3} + \frac{V_c - V_t}{R_5} + \frac{V_c}{R_4} = 0$$

KCL @ d:

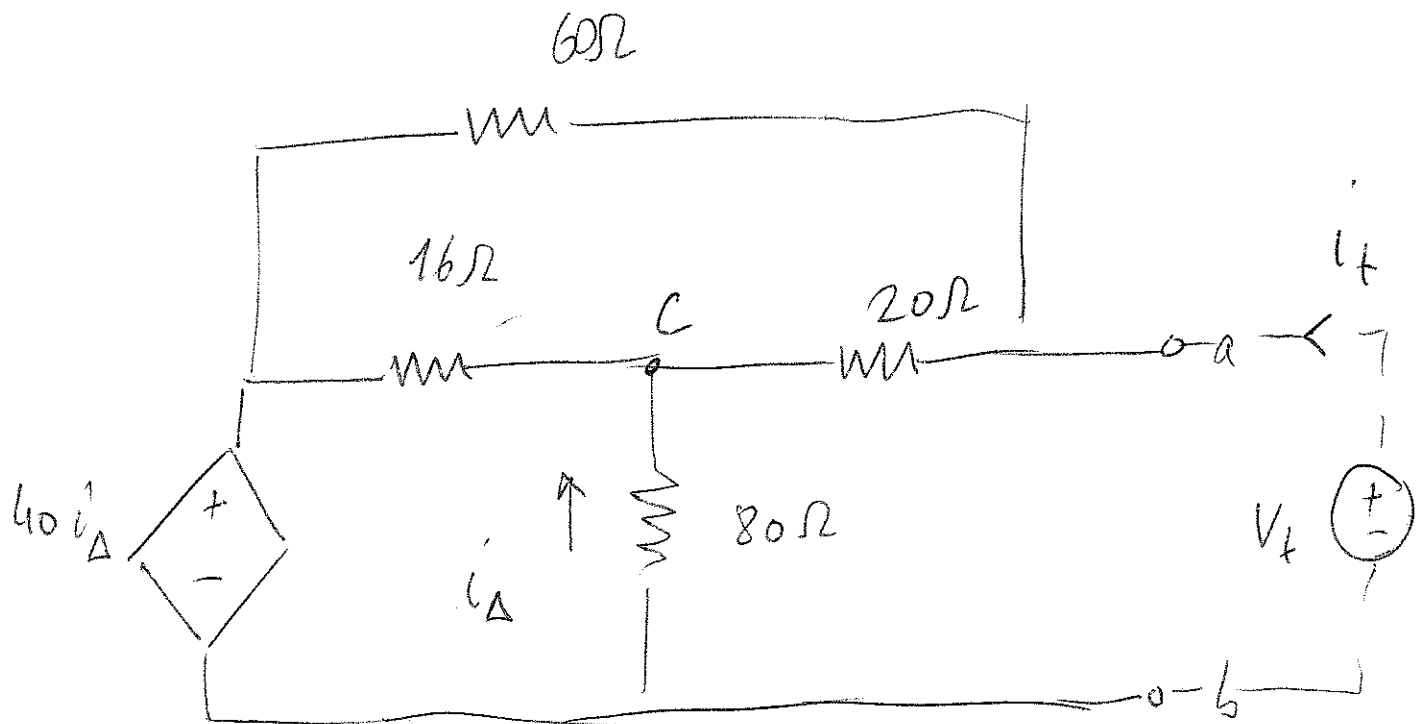
$$\frac{V_d - V_t}{R_1} + \frac{V_d - V_c}{R_3} + \frac{V_d}{R_2} = 0$$

now give V_t a value like 1V &
solve for V_c & V_d .

$$i_+ = \cancel{V_d} - \left(\frac{V_c - V_t}{R_5} + \frac{V_d - V_t}{R_1} \right) \left[\begin{array}{l} \text{KCL} \\ @ a \end{array} \right]$$



Slide 34 :



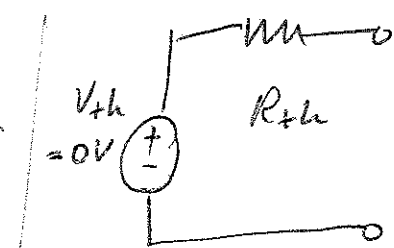
$$V_{oc} = 0, \quad I_{sc} = 0 \quad R_{th} = \frac{V_{oc}}{I_{sc}} = ?$$

KCL @ C

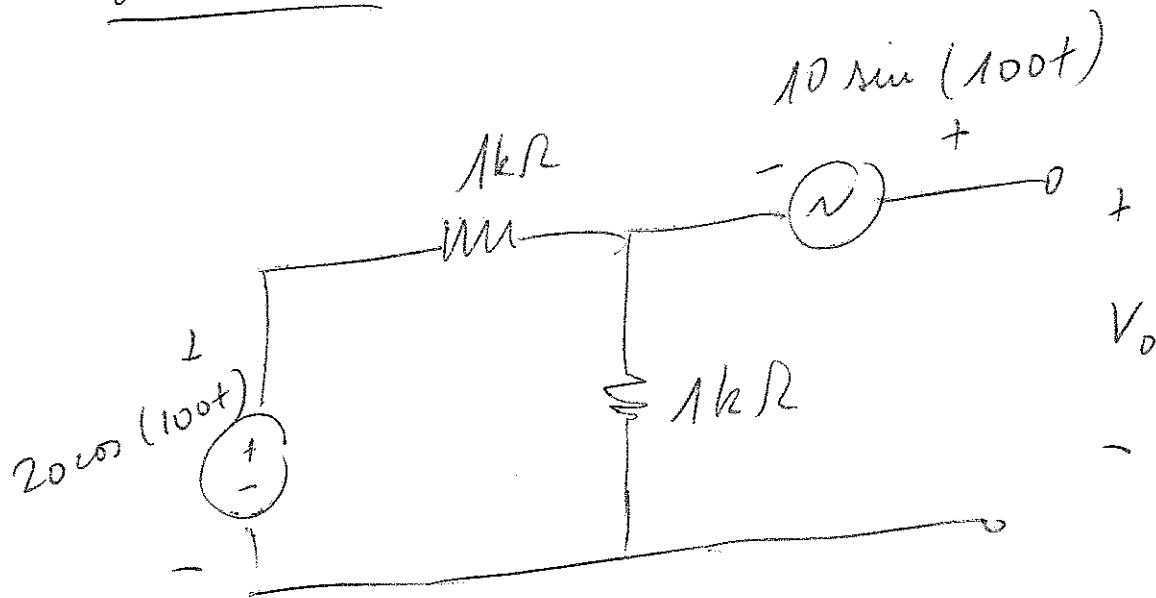
$$\left. \begin{array}{l} 2 \text{ eq} \\ 2 \text{ unknown} \end{array} \right\} \begin{cases} \frac{V_c - 40i_\Delta}{16} + \frac{V_c}{80} + \frac{V_c - V_t}{20\Omega} = 0 \\ i_\Delta = -\frac{V_c}{80\Omega} \end{cases}$$

Solve for V_c by making V_t like 1V.

Solve for i_t & $R_{th} = \frac{V_t}{i_t}$



Slide 35

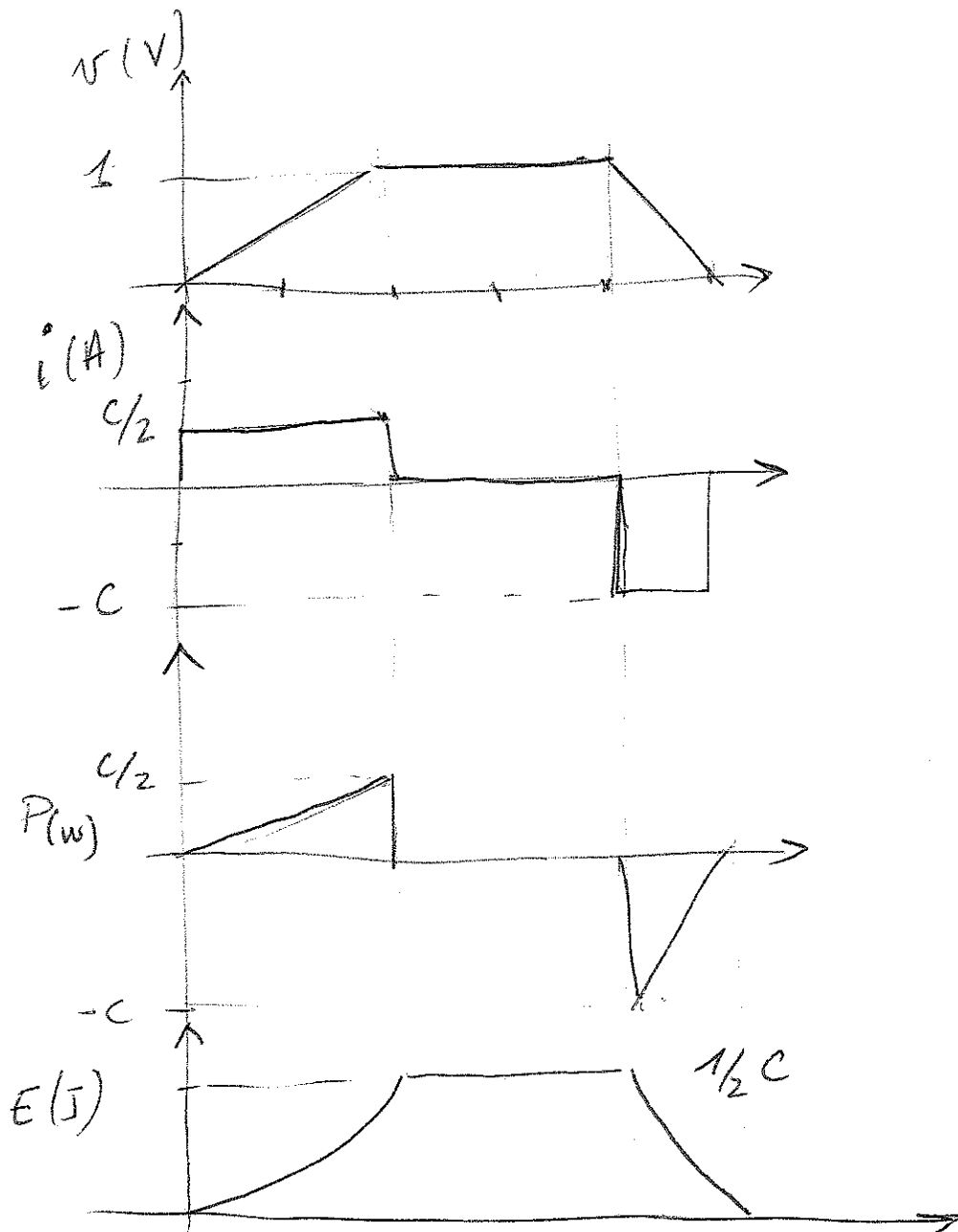


By superposition: $V_o = 10\cos(100t) + 10\sin(100t)$

Lecture 4

slide 3: previously done in another lecture.

slide 10:



Slide 12

$$V_1(t) = \frac{1}{C_1} \int i'(t) dt + \frac{Q_1}{C_1}$$

$$V_2(t) = \frac{1}{C_2} \int i'(t) dt + \frac{Q_2}{C_2}$$

$$V(t) = V_1(t) + V_2(t) = \left(\frac{1}{C_1} + \frac{1}{C_2} \right) \int i'(t) dt + \frac{Q_1}{C_1} + \frac{Q_2}{C_2}$$

$V(t)$ also equals:

$$V(t) = \frac{1}{C_{eq}} \int i'(t) dt + \frac{Q_{eq}}{C_{eq}}$$

$$\Rightarrow \frac{1}{C_{eq}} = \frac{1}{C_1} + \frac{1}{C_2}$$

$$Q_{eq} = C_{eq} \left[\frac{Q_1}{C_1} + \frac{Q_2}{C_2} \right]$$

Slide 13

$$i_1(t) = C_1 \frac{dV(t)}{dt}$$

$$i_2(t) = C_2 \frac{dV(t)}{dt}$$

$$i(t) = i_1(t) + i_2(t) = (C_1 + C_2) \frac{dV(t)}{dt}$$

$$i(t) \text{ also equals: } i(t) = C_{eq} \frac{d(V(t))}{dt}$$

$$\Rightarrow \underline{C_{eq} = C_1 + C_2}$$

Slide 16:

$$p(t_0) = v(t_0) i'(t_0) = L \frac{di'(t_0)}{dt} \cdot i'(t_0)$$

$$= L \frac{di'(t_0)}{dt} \cdot i_0$$

$$w(t) = \int_{t_0}^t p(\tau) d\tau = \int_{t_0}^t v(\tau) i'(\tau) d\tau = \int_{t_0}^t L \frac{di'(\tau)}{d\tau} i'(\tau) d\tau$$

$$= \int_{t_0}^t L i'(\tau) d\tau = \frac{1}{2} L i^2 - \frac{1}{2} L i_0^2$$

Slide 17:

$$v_1(t) = L_1 \frac{di'(t)}{dt}$$

$$v_2(t) = L_2 \frac{di'(t)}{dt}$$

$$v(t) = v_1(t) + v_2(t) = (L_1 + L_2) \frac{di'(t)}{dt}$$

$v(t)$ also equals:

$$v(t) = L_{eq} \frac{di'(t)}{dt} \Rightarrow L_{eq} = L_1 + L_2$$

Slide 18:

$$i_1(t) = \frac{1}{L_1} \int v(t) dt + i_1(0)$$

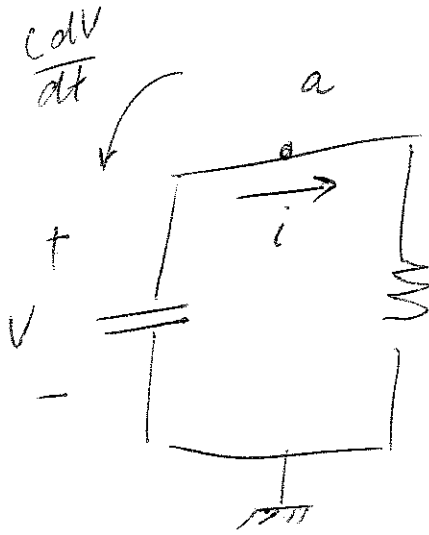
$$i_2(t) = \frac{1}{L_2} \int v(t) dt + i_2(0)$$

$$i'(t) = i_1(t) + i_2(t) = \left[\frac{1}{L_1} + \frac{1}{L_2} \right] \int v(t) dt + i_1(0) + i_2(0)$$

$i'(t)$ also equals:

$$i'(t) = \frac{1}{L_{eq}} \int v(t) dt + i_{eq}(0) = \begin{cases} \frac{1}{L_{eq}} = \frac{1}{L_1} + \frac{1}{L_2} \\ i_{eq}(0) = i_1(0) + i_2(0) \end{cases}$$

Slide 29:



KCL :

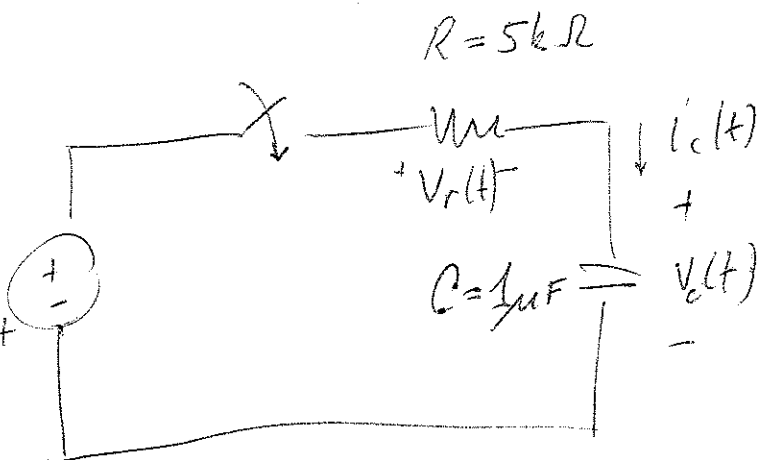
$$+ \frac{C dV}{dt} + V/R = 0$$

$$\Rightarrow V(t) + RC \frac{dV(t)}{dt} = 0$$

Lecture 5:

slide 9:

$$V_s(t) = 2 \sin 200t$$



KVL:

$$-V_s(t) + V_R(t) + V_C(t) = 0$$

$$RC \frac{dV_C(t)}{dt} + V_C(t) = V_s(t)$$

Complementary solution: $K e^{st}$ for $RC \frac{dV_C(t)}{dt} + V_C(t) = 0$ yields $K = 0$ since the DC value of $V_C(t)$ stays at 0V.

Particular solution:

$$(1) \quad RC \frac{dV_C(t)}{dt} + V_C(t) = 2 \sin 200t$$

$V_C(t)$ is of the form: $A \cos 200t + B \sin 200t$

replace back into 1:

$$RC \cdot [-200 A \sin 200t + B 200 \cos 200t]$$

$$+ A \cos 200t + B \sin 200t = 2 \sin 200t$$

$$\Rightarrow \begin{cases} -200 A RC + B = 2 \\ RC \cdot B \cdot 200 + A = 0 \end{cases}$$

solve for A & B

Lecture 6
Slide 24:

$$v(t) = 120V \cos(377t + 30^\circ)$$

$$V = 120 \angle 30^\circ$$

$$I = \frac{V}{Z_C} \quad Z_C = \frac{1}{j\omega C}$$

$$\Rightarrow I = j\omega C \cdot V$$

$$= \omega C \cdot |V| \angle (\angle V + 90^\circ)$$

$$\Rightarrow i(t) = \omega C \cdot 120V \cos(377t + 120^\circ)$$

$$\text{where } \omega = 377 \frac{\text{rad}}{\text{s}}$$

Slide 26:

$$i(t) = 1\mu A \cos(2\pi \cdot 9.15 \cdot 10^7 t + 30^\circ)$$

$$I = 1\mu \angle 30^\circ$$

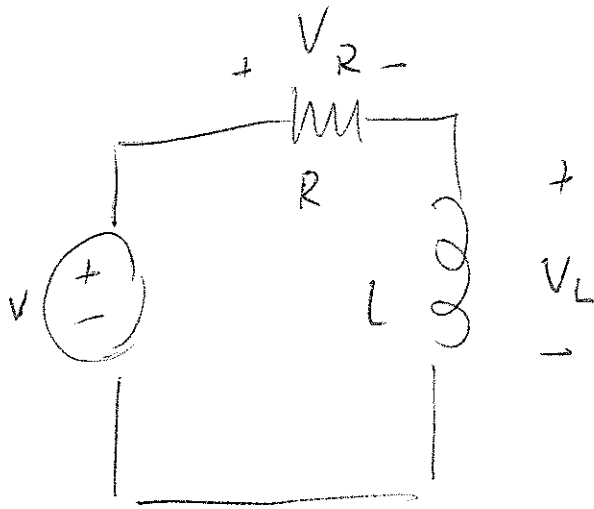
$$Z_L = j\omega L$$

$$V = I \cdot Z = j\omega L \cdot 1\mu \angle 30^\circ$$

$$= \omega \cdot L \cdot 1\mu \angle 30 + 90$$

$$v(t) = \omega L \cdot 1\mu A \cos(\omega t + 120^\circ)$$

Lecture 7 :



1st Order Lowpass filter:

$$H(j\omega) = \frac{V_R}{V} = \frac{R}{R + j\omega L}$$

$$H(j\omega) = \frac{1}{1 + j\omega \frac{L}{R}} = \frac{1}{1 + j\frac{\omega}{\omega_B}}$$

$$\text{where } \omega_B = \frac{R}{L}$$

1st Order highpass filter:

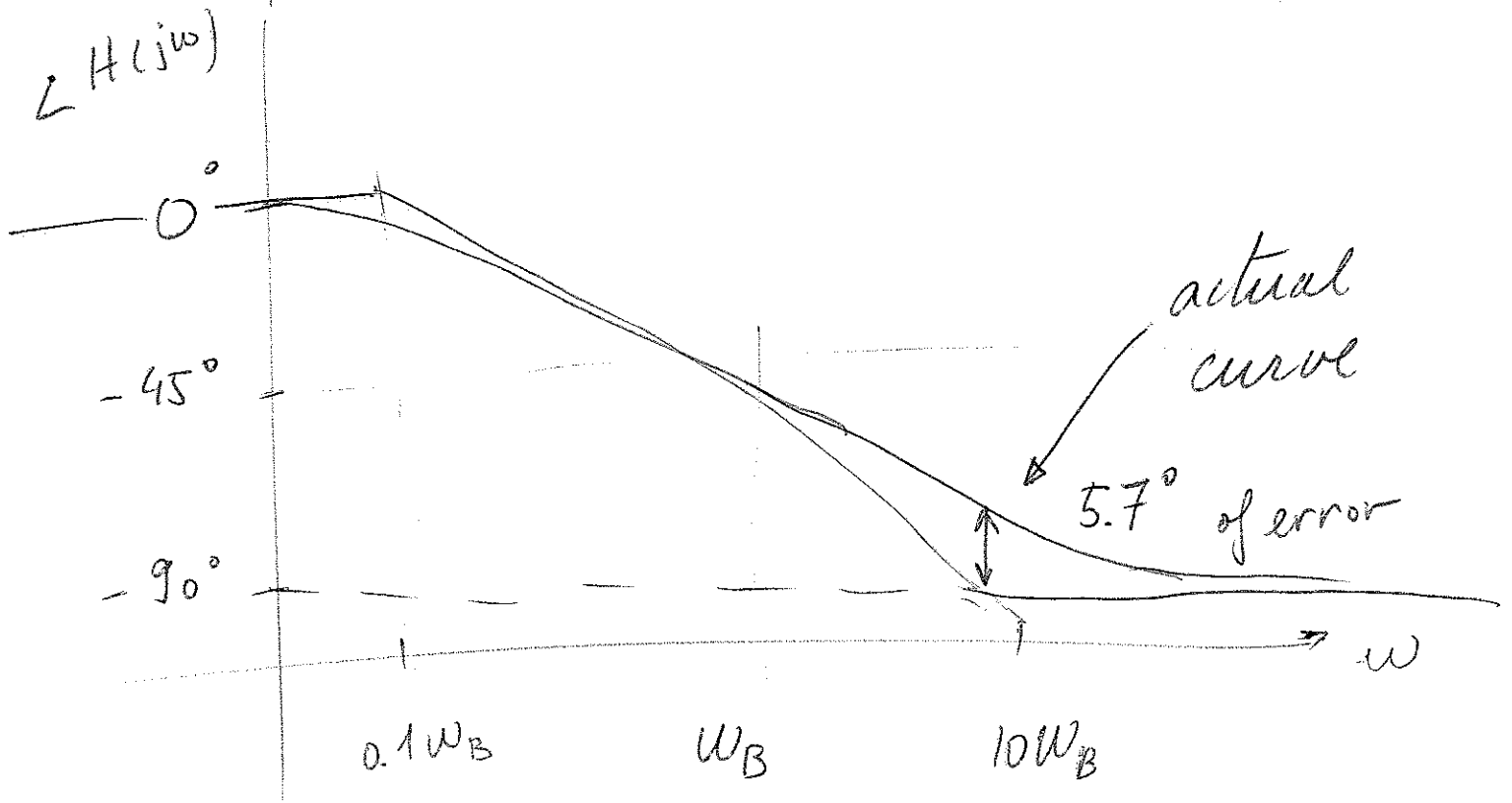
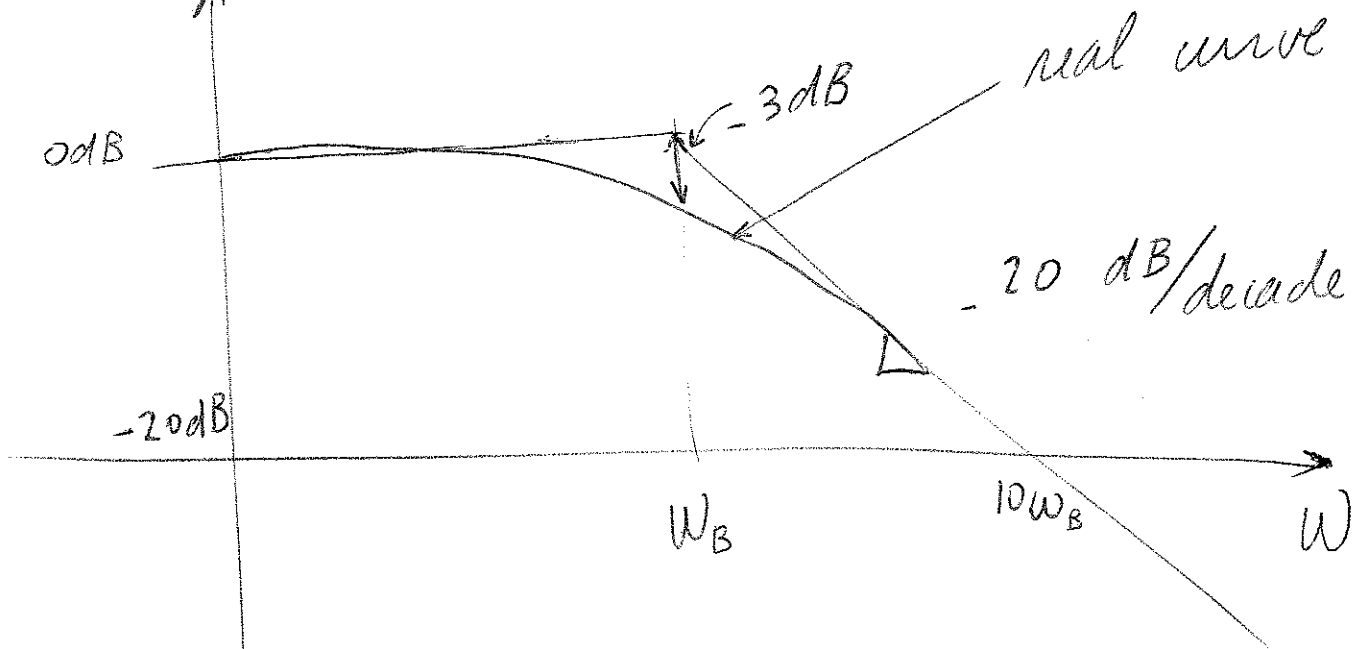
$$H(j\omega) = \frac{V_L}{V} = \frac{j\omega L}{R + j\omega L} = \frac{j\omega \frac{L}{R}}{1 + j\omega \frac{L}{R}}$$

$$H(j\omega) = \frac{j\frac{\omega}{\omega_B}}{1 + j\frac{\omega}{\omega_B}} \quad \text{where } \omega_B = \frac{R}{L}$$

Bode Plot:

$$H(j\omega) = \frac{1}{1 + j \frac{\omega}{\omega_B}} = \sqrt{\frac{1}{1 + \left(\frac{\omega}{\omega_B}\right)^2}} \angle -\tan^{-1} \frac{\omega}{\omega_B}$$

$$20 \log(|H(j\omega)|)$$



Bode plot of high pass filter:

$$H(j\omega) = \frac{j\omega/\omega_B}{1 + j\omega/\omega_B}$$

$$H(j\omega) = \frac{\omega/\omega_B}{\sqrt{1 + (\frac{\omega}{\omega_B})^2}} \angle \frac{\pi}{2} - \tan^{-1}\left(\frac{\omega}{\omega_B}\right)$$

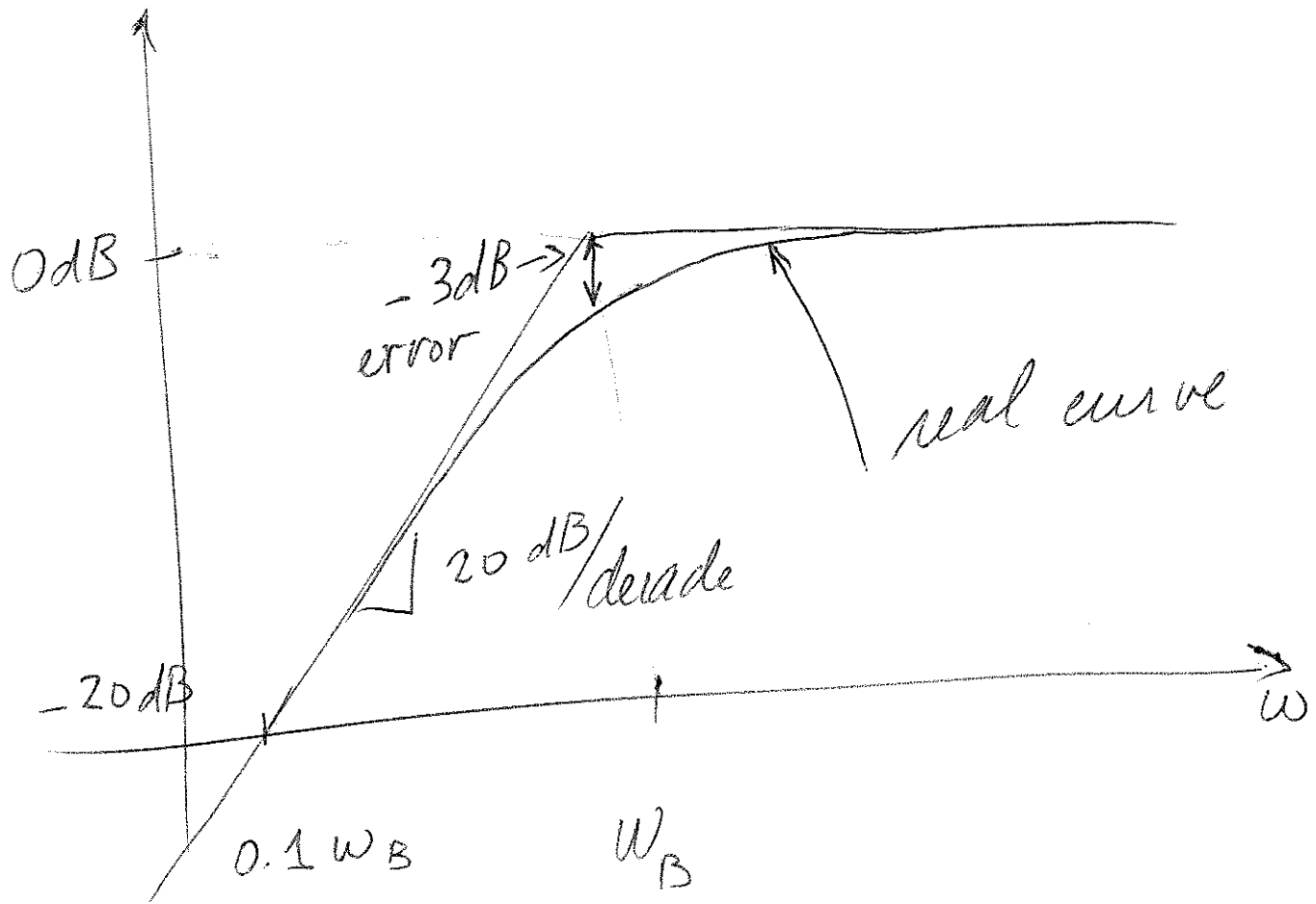
Magnitude plot:

$$|H(j\omega_B)| = \frac{1}{\sqrt{2}} \equiv -3\text{dB}$$

$$\text{for } \omega \gg \omega_B, |H(j\omega)| \approx 1 \equiv 0\text{dB}$$

$$\text{for } \omega \ll \omega_B, |H(j\omega)| \approx \frac{\omega}{\omega_B} \equiv \text{slope of } +20\text{dB/decade}$$

Magnitude Plot of high pass filter:

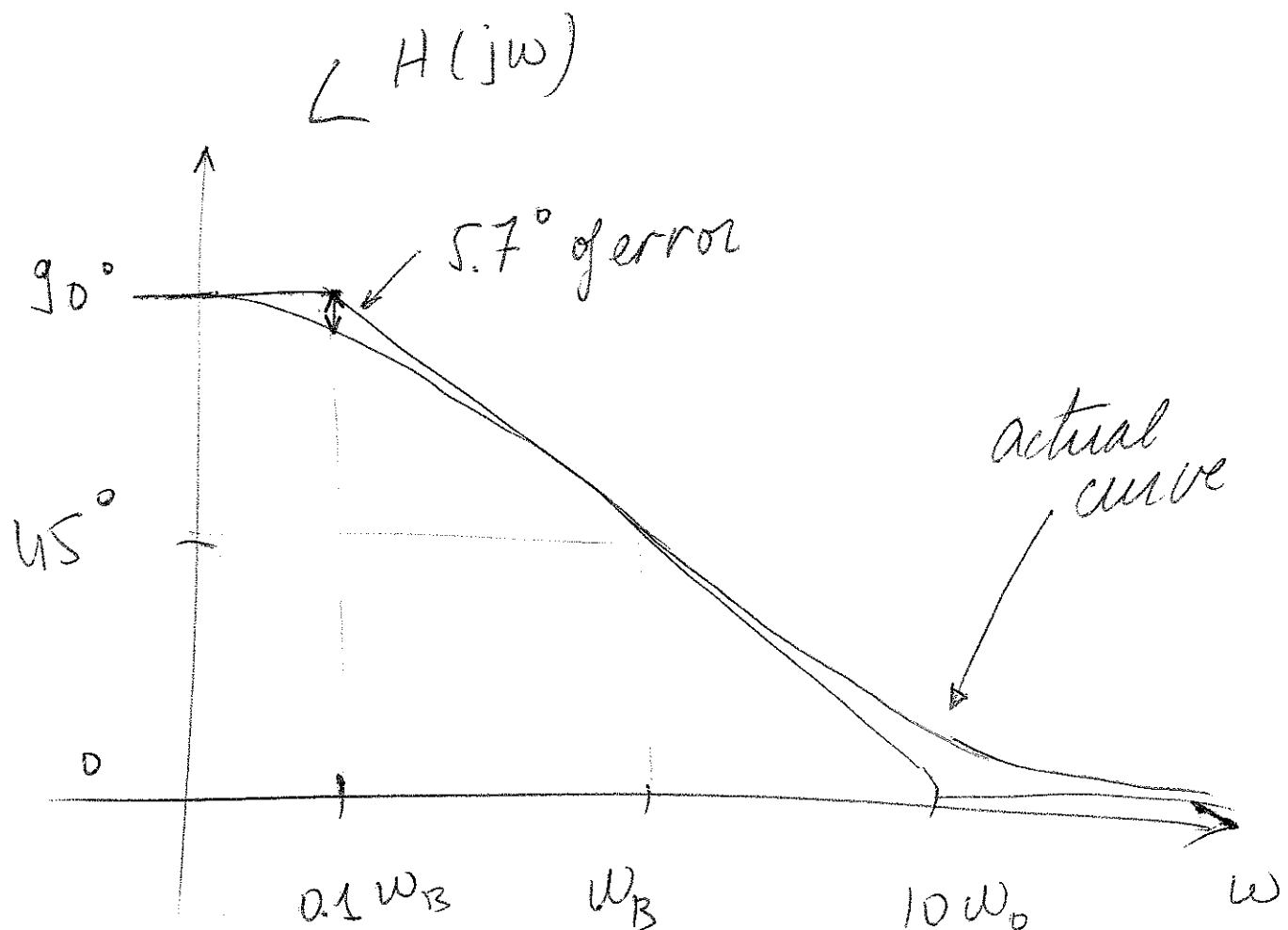


Phase plot of high pass filter.

$$\angle H(j\omega_B) = 45^\circ$$

$$\angle H(j 0.1 \omega_B) = 84.3^\circ \approx 90^\circ$$

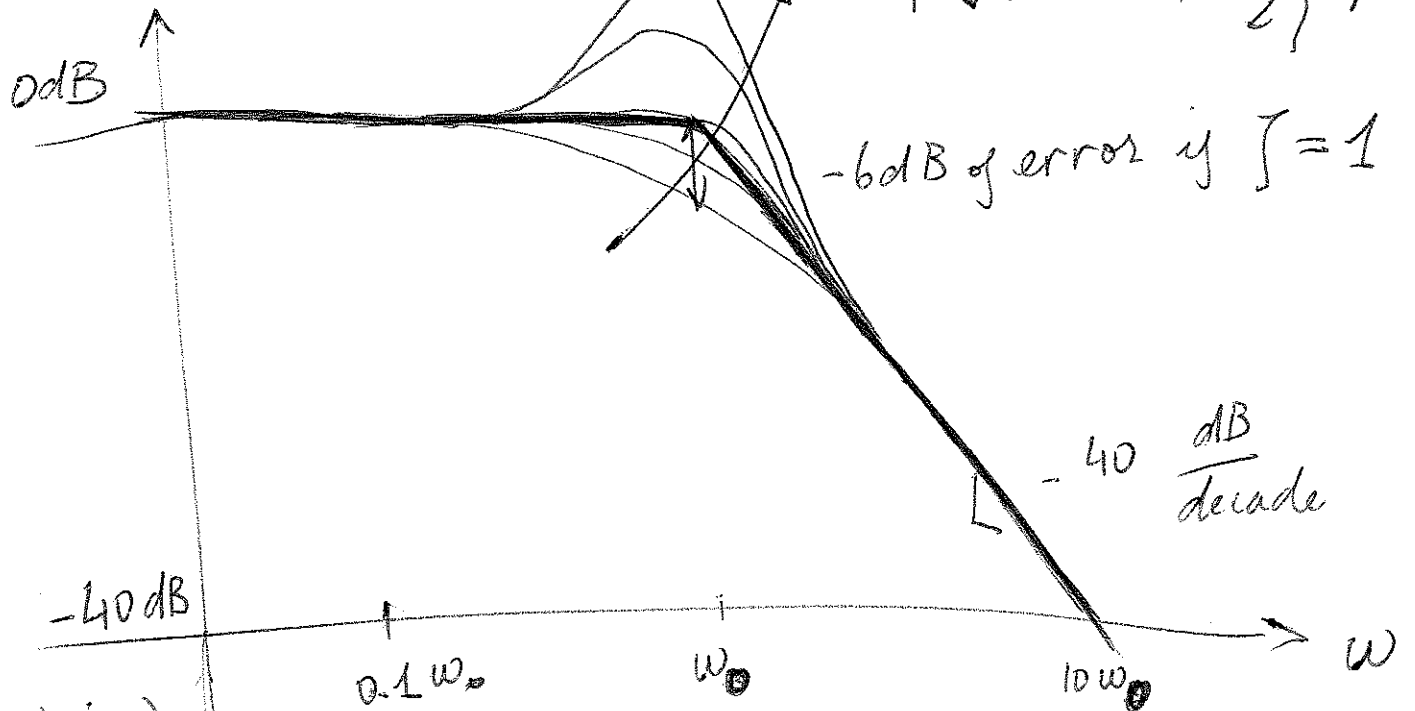
$$\angle H(j 10 \omega_B) = 5.7^\circ \approx 0^\circ$$



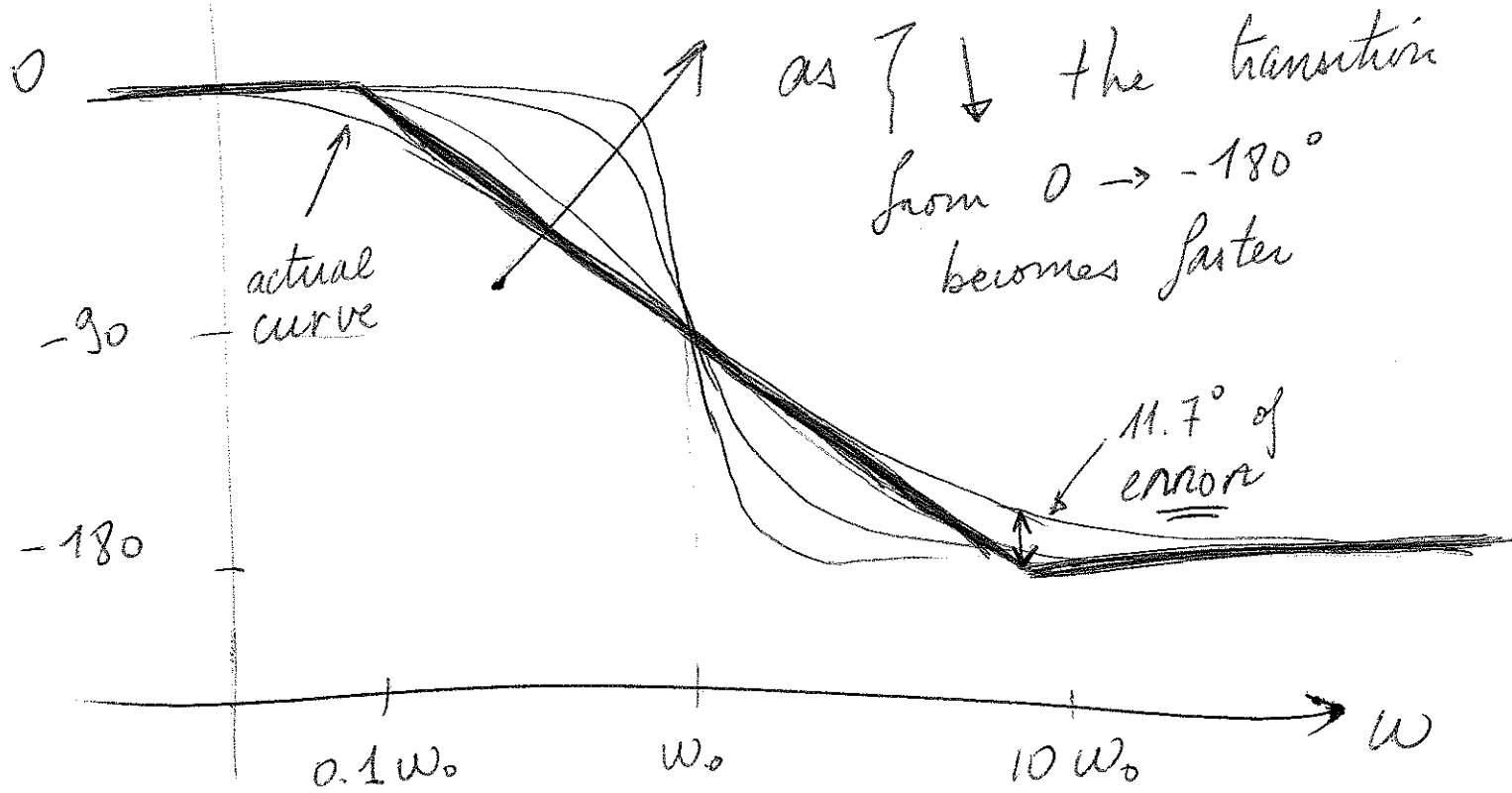
Bode plot of second order low pass filter.

for $\zeta < 1$

$$20 \log (|H(j\omega)|)$$



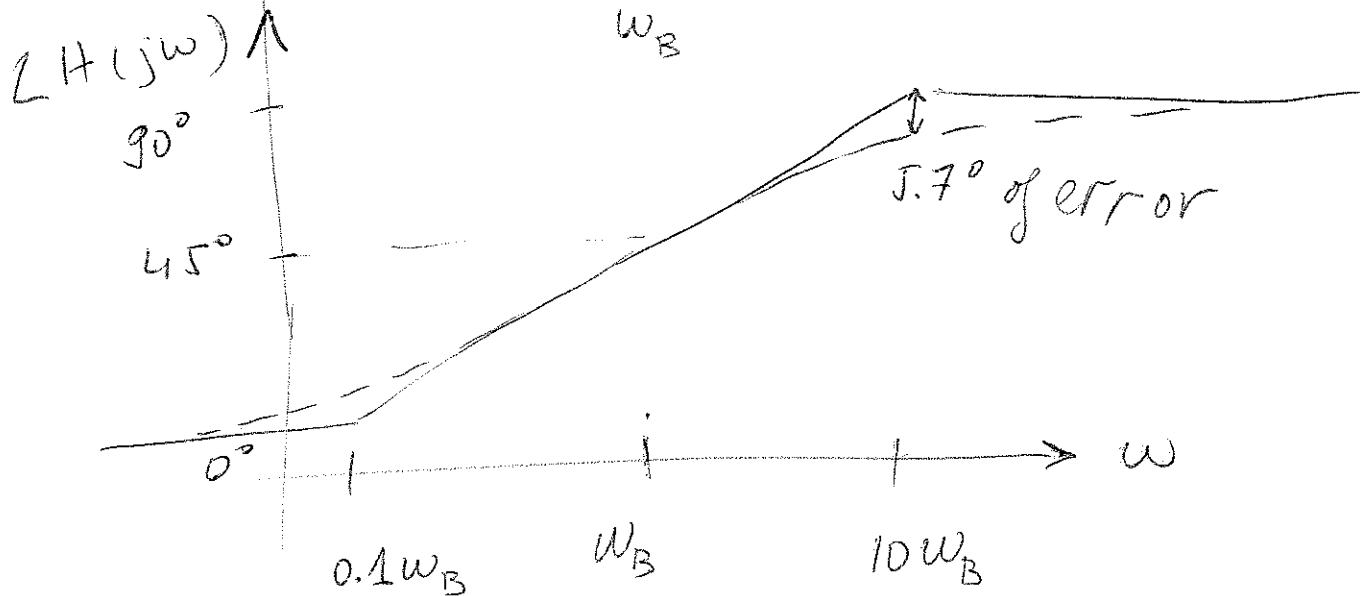
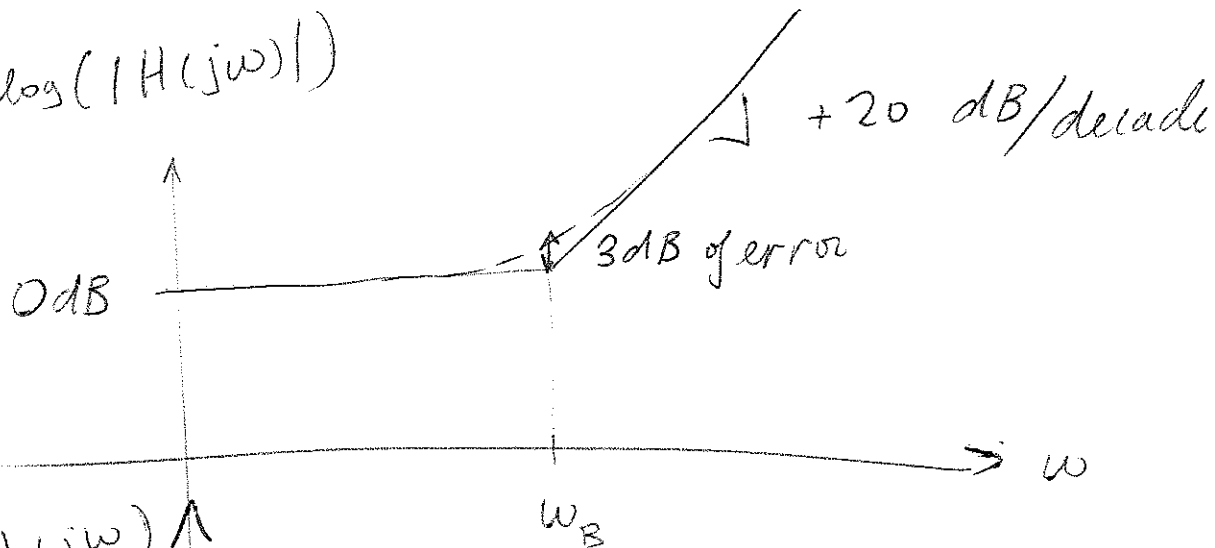
$\angle H(j\omega)$



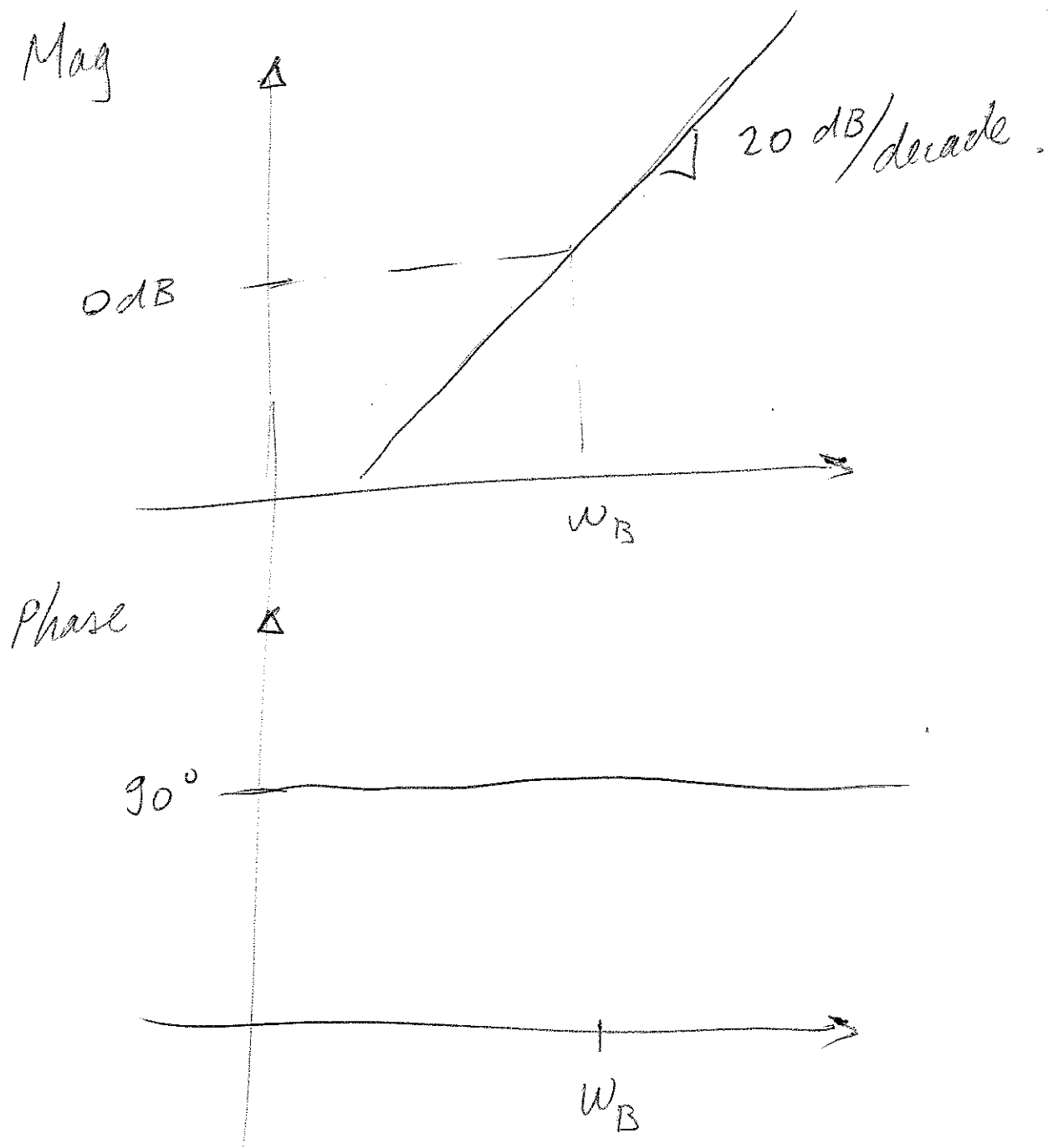
Higher Order Bode plots:

For: $H(j\omega) = 1 + \frac{j\omega}{\omega_B}$

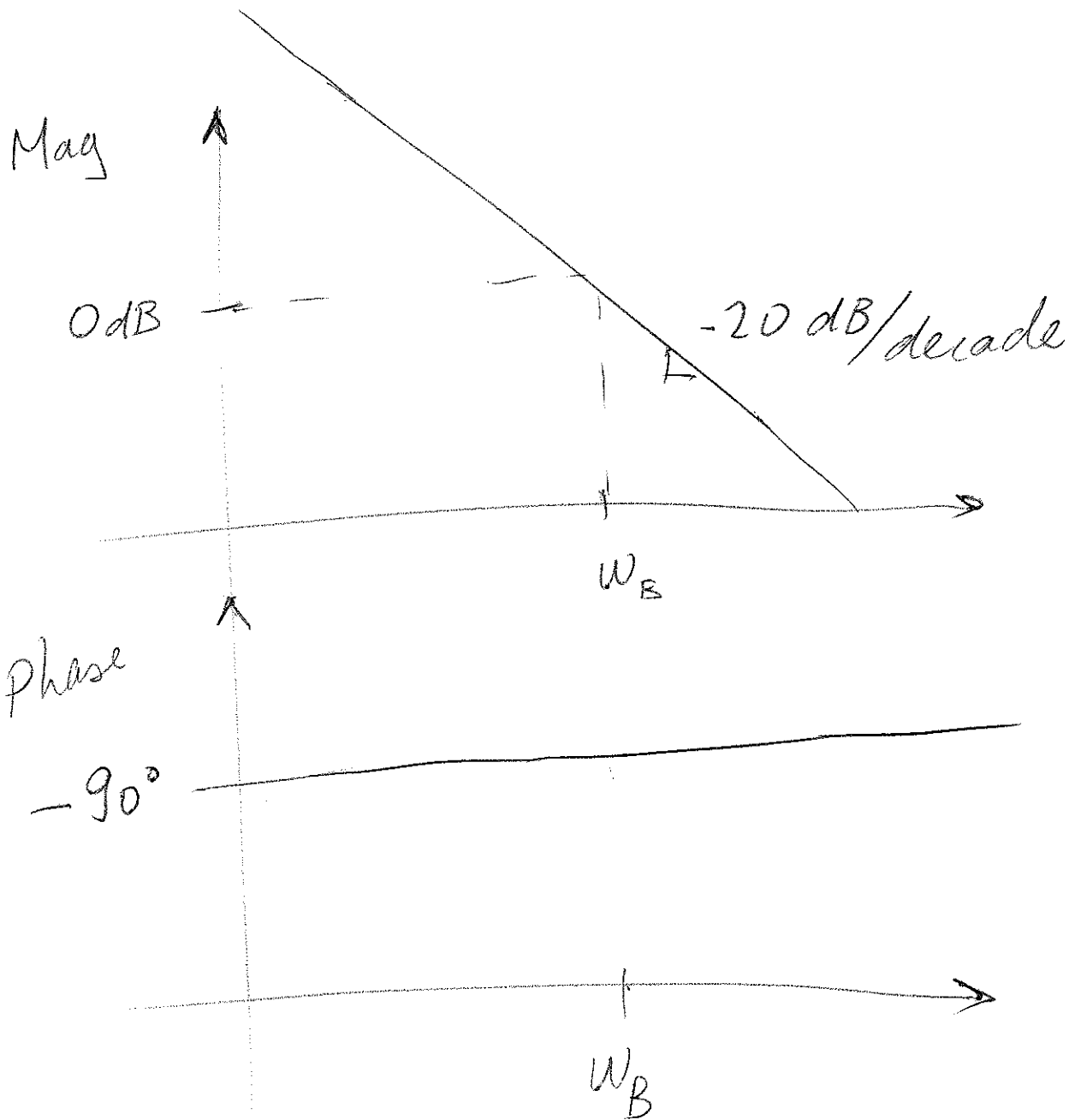
$$20 \log(|H(j\omega)|)$$

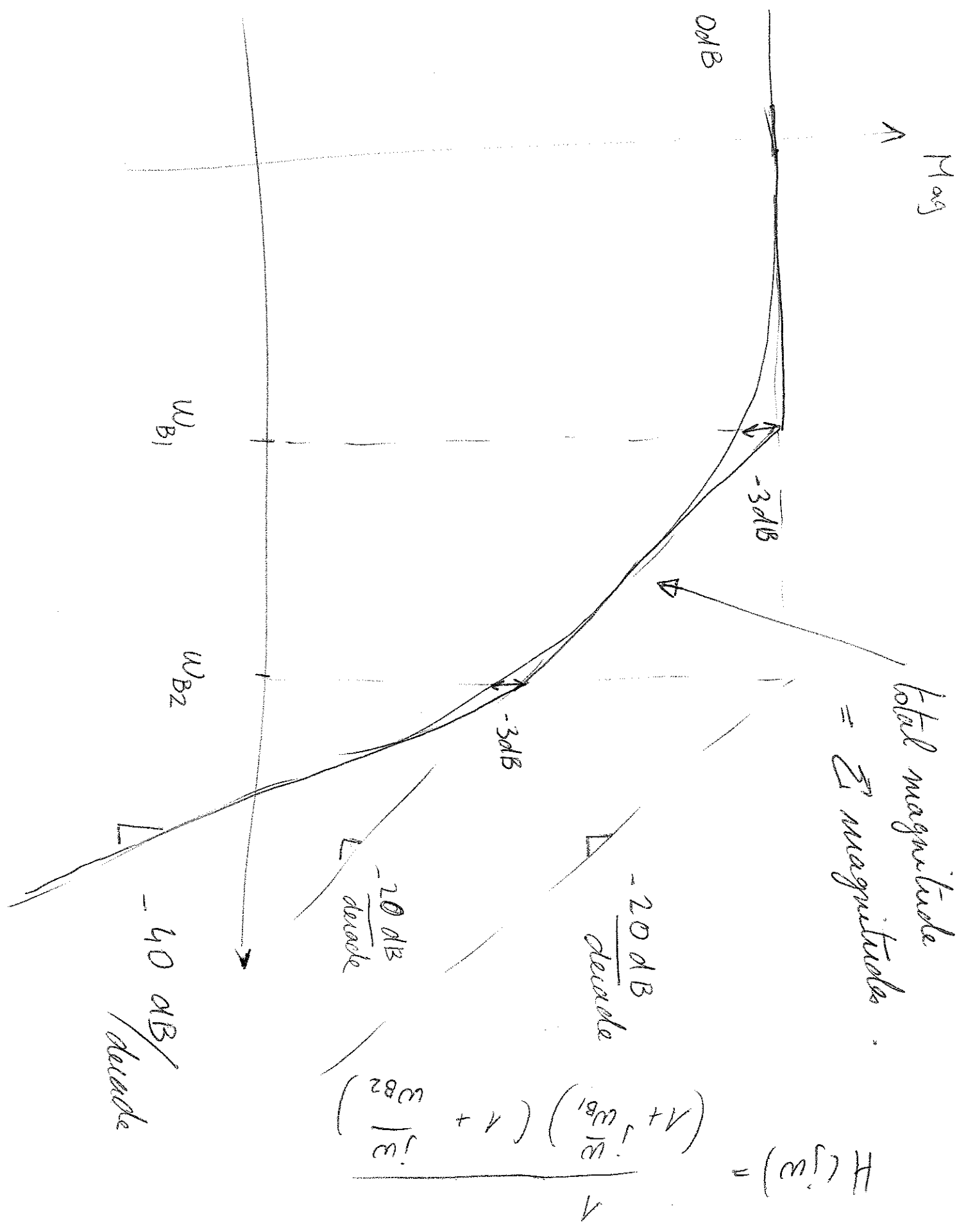


For $H(j\omega) = j\omega/\omega_B$

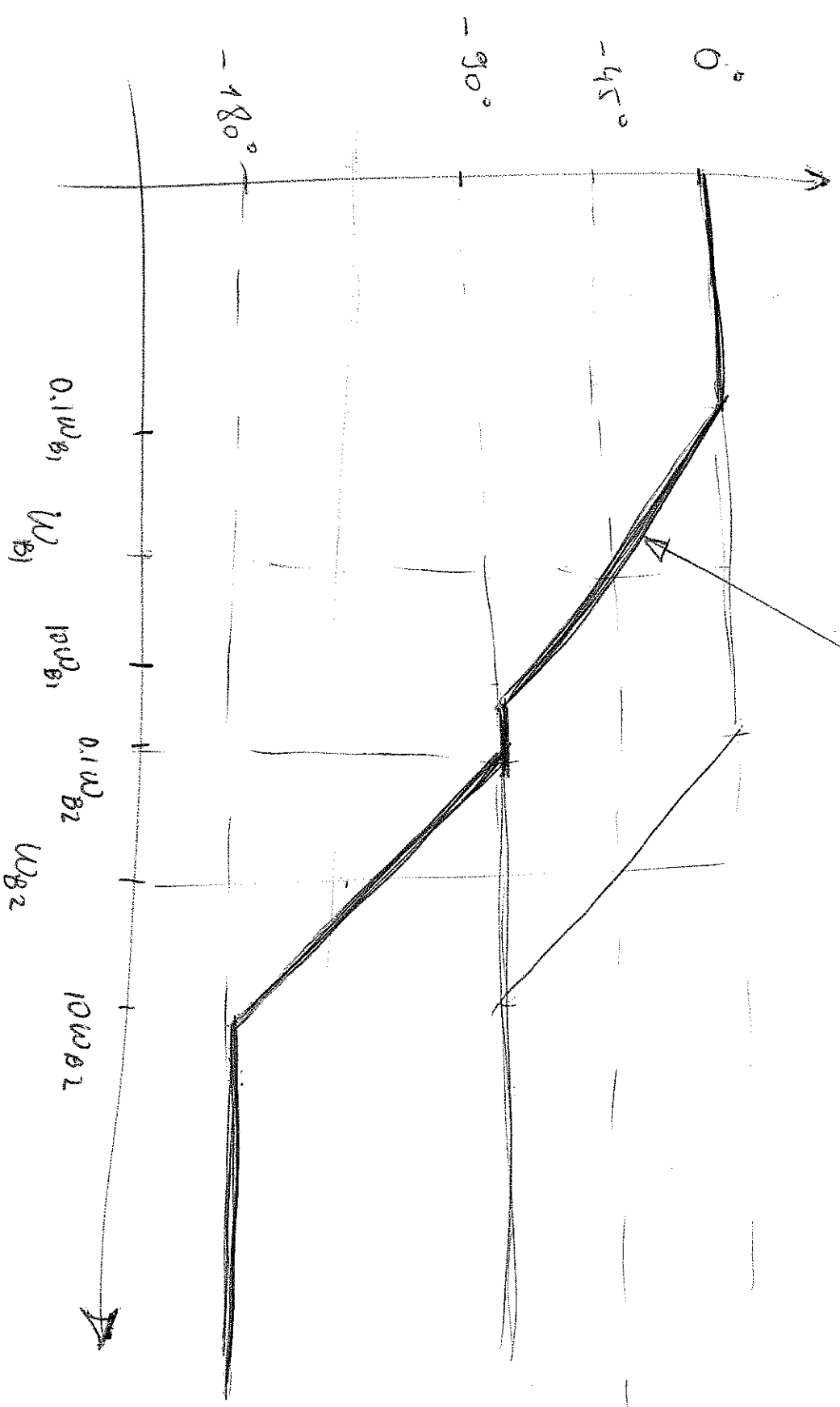


For $H(j\omega) = j \frac{1}{\omega/\omega_B}$



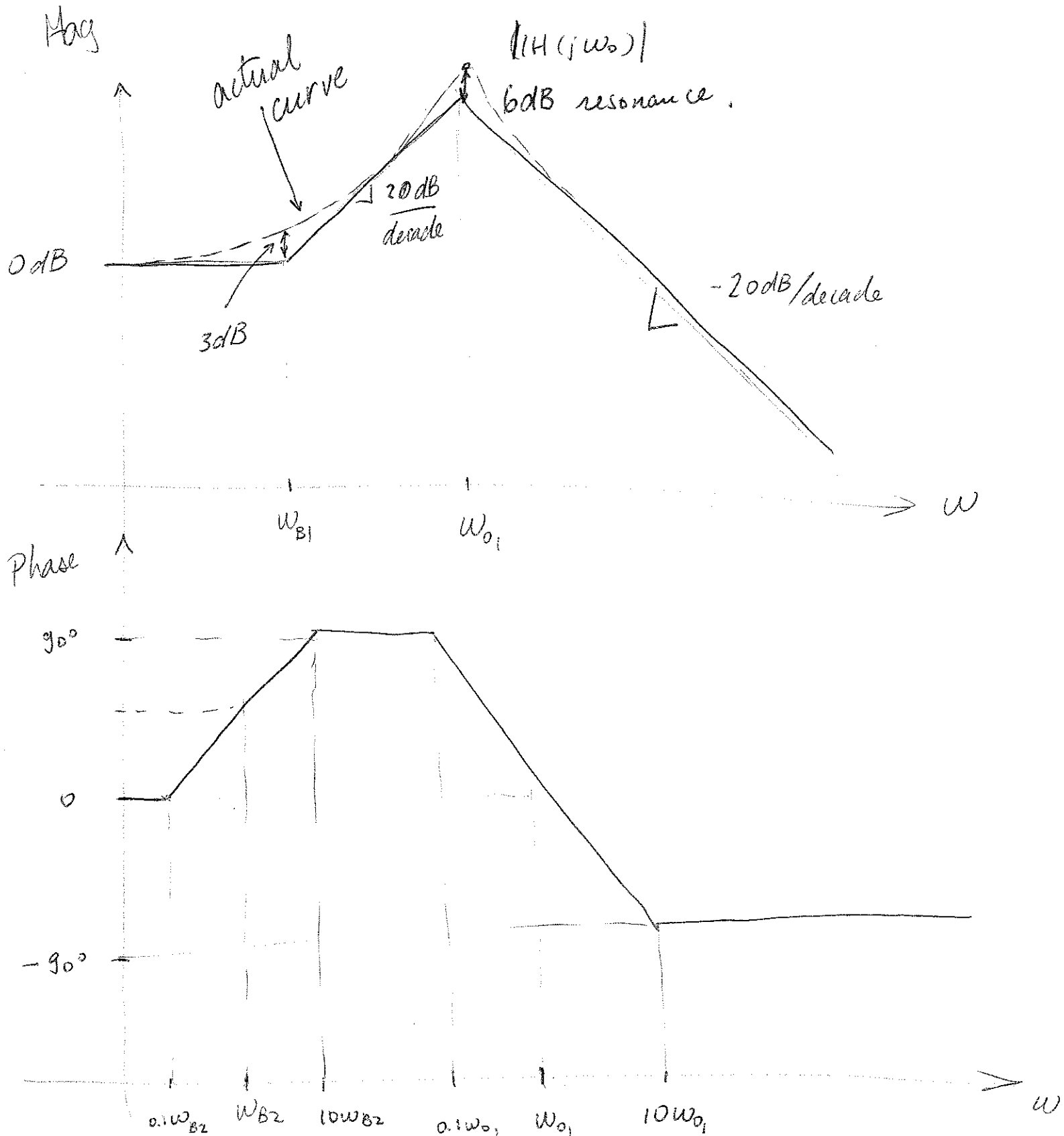


Phase



$$H(j\omega) = \frac{(1 + j\frac{\omega}{\omega_B})}{1 + 2\zeta j\frac{\omega}{\omega_0} + (\frac{j\omega}{\omega_0})^2}$$

$$\zeta = 1/4$$



Lecture 8:

slide 3: $L_{eq} = \left(\frac{1}{L_1} + \frac{1}{L_2} \right)^{-1} + L_3$

$$Z_{eq} = \left(\frac{1}{j\omega L_1} + \frac{1}{j\omega L_2} \right)^{-1} + j\omega L_3$$

slide 4: $C_{eq} = \left(\frac{1}{C_1 + C_2} + \frac{1}{C_3} \right)^{-1}$

$$Z_{eq} = \frac{1}{j\omega C_3} + \left[j\omega C_1 + j\omega C_2 \right]^{-1}$$

~~$\Delta V_o = \Delta V_i$~~

$$\Delta Q = \Delta V_i \cdot C_{eq}$$

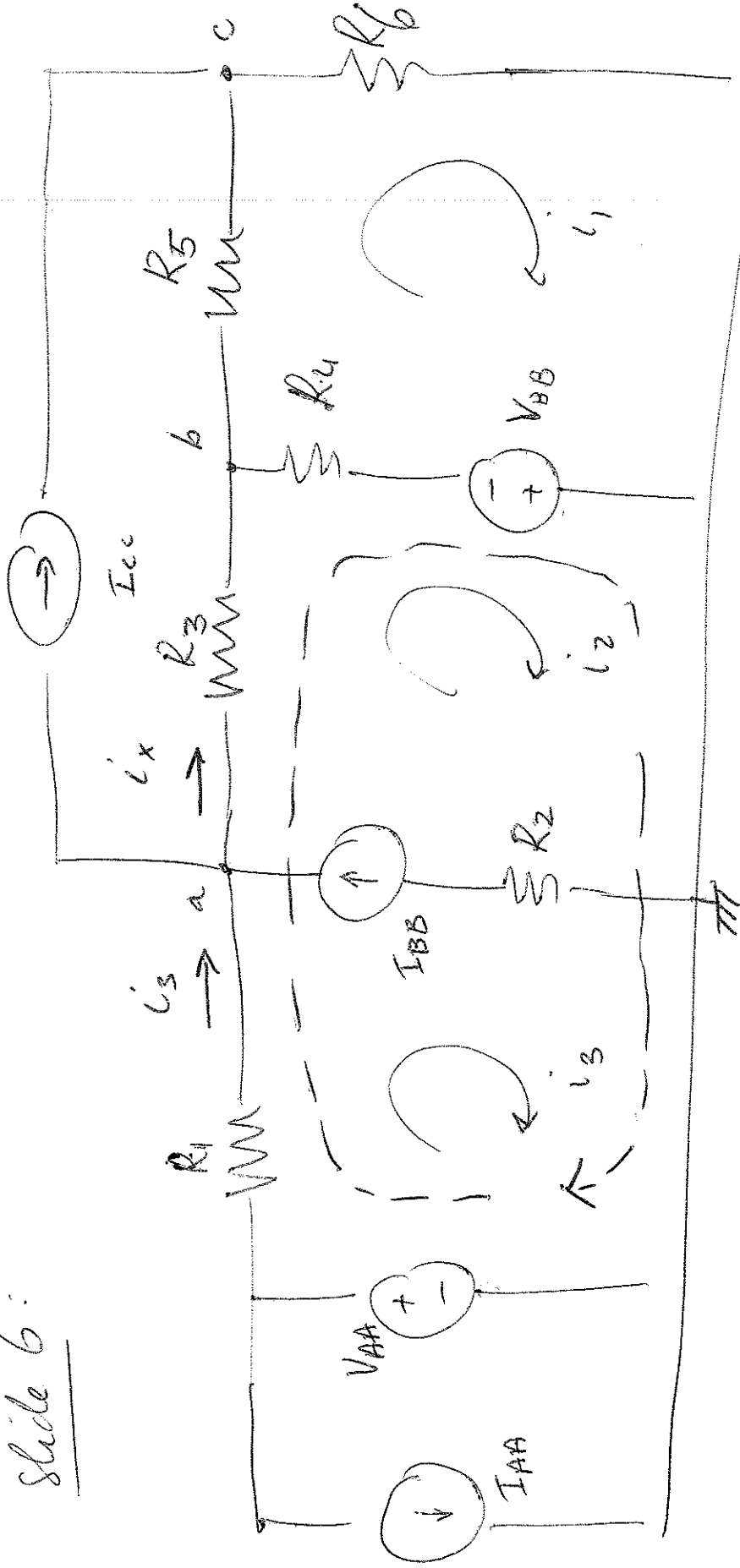
$$\Delta V_o = \frac{\Delta Q}{C_3} = \Delta V_i \cdot \frac{C_{eq}}{C_3}$$

slide 5: $Q_1 = C_1 \cdot V_1$ $Q_2 = C_2 \cdot V_2$

$$Q_{total} = Q_1 + Q_2$$

$$V_{final} = \frac{Q_{total}}{C_{eq}} = \frac{C_1 V_1 + C_2 V_2}{C_1 + C_2}$$

slide 6:



$$\text{KVL @ } i_1: V_{BB} + (i_1 - i_2) R_4 + (i_1 - I_{CC}) R_5 + i_1 R_6 = 0V$$

KVL @ supermesh:

$$-V_{AA} + i_3 R_1 + (i_2 - I_{CC}) R_3 + (i_2 - i_1) R_4 + (-V_{BB}) = 0V$$

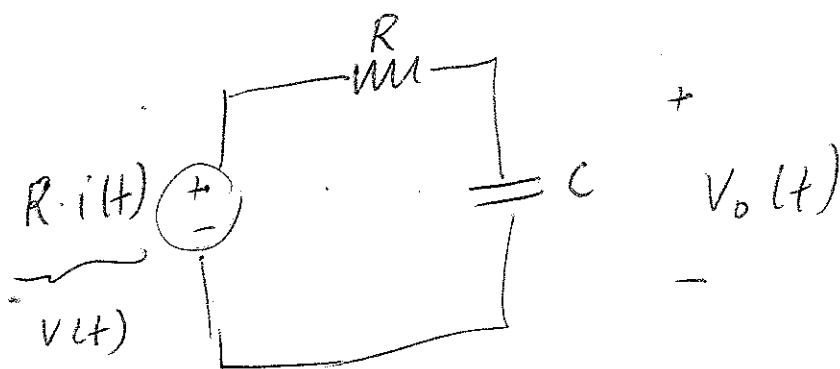
we need one more equation

$$\text{KCL @ } a: -i_3 + I_{CC} + i_x - I_{BB} = 0 \quad \text{where } i_x = i_2 - I_{CC}$$

$$\Rightarrow I_{BB} = i_2 - i_3$$

Slide 7 :

using a source transformation, the circuit becomes:



$$V(t) = 2 + 3\mu(t).$$

Solution 1:

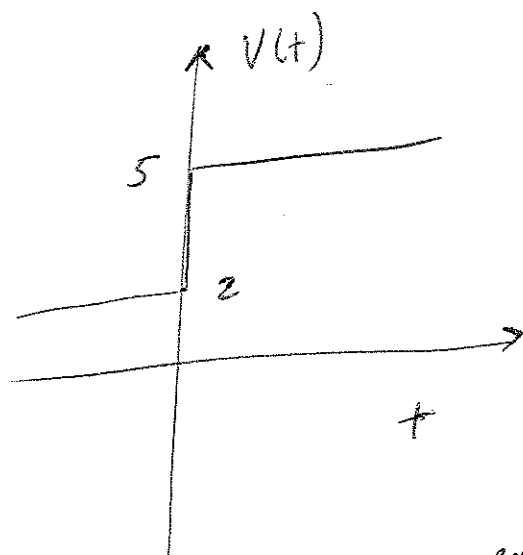
$$\text{KVL: } -v(t) + R \cdot i'(t) + V_o(t) = 0$$

$$i'(t) = \frac{C dV_o(t)}{dt}$$

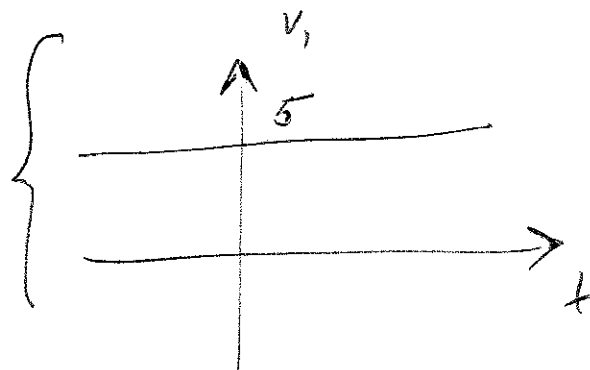
$$\Rightarrow V_o(t) + RC \frac{dV_o(t)}{dt} = V(t)$$

$$V_o(t) = \underbrace{V_c(t)}_{\text{complementary solution}} + \underbrace{V_p(t)}_{\text{particular solution}}$$

$$V(t) = 2 + 3u(t)$$

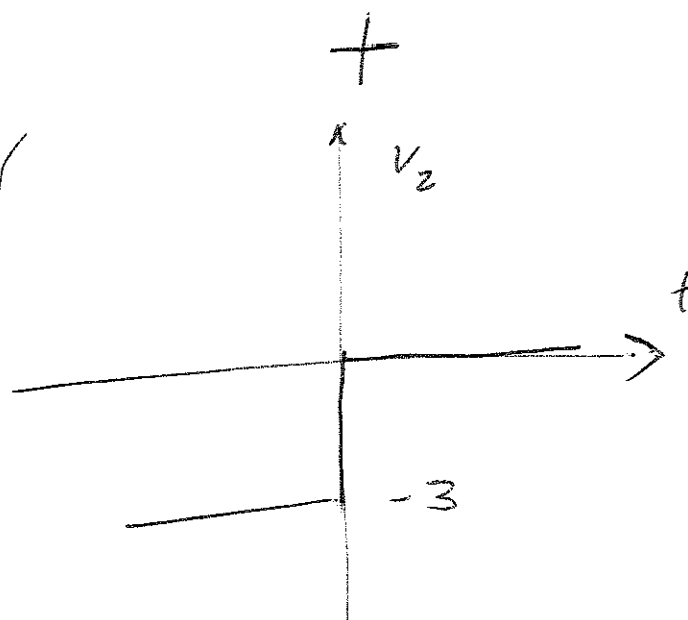


used
to find
 $V_p(t)$



used
to find
 $V_c(t)$

=



for $t \geq 0$

$$V_c(t) + RC \frac{dV_c(t)}{dt} = 0$$

$$V_c(t) = K e^{-t/\tau}$$

we know that $V_c(0) = -3V$

$$\Rightarrow V_c(t) = -3e^{-t/\tau} \quad \text{where } \tau = RC$$

also we know $V_p(t) = 5$

$$\Rightarrow V_o(t) = V_c(t) + V_p(t) = 5 - 3e^{-t/\tau}$$

Solution 2:

$$V_o(t) + RC \frac{dV_o(t)}{dt} = v(t)$$

$$V_o(t) = K_1 + K_2 e^{-t/\tau}$$

Initial conditions:

$$V_o(0) = 2V \Rightarrow K_1 + K_2 = 2$$

$$\lim_{t \rightarrow \infty} V_o(t) = 5V \Rightarrow K_1 = 5V$$

$$\Rightarrow V_o(t) = 5 - 3e^{-t/\tau}$$

Solution 3:

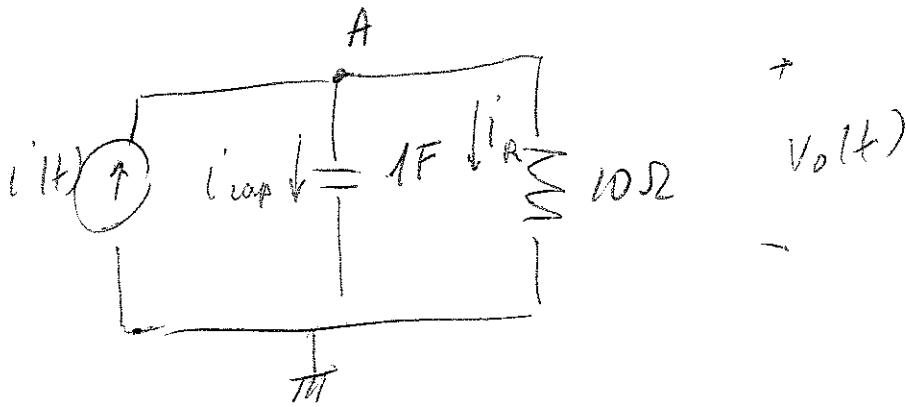
$$V_o(t) = V_f - (V_f - V_i) e^{-t/\tau}$$

$$V_f = 5V \quad V_i = 2V$$

$$\Rightarrow V_o(t) = 5 - 3e^{-t/\tau} \quad \text{where } \tau = RC$$

Slide 7:

1st Order Circuit:



KCL @ A: $-i'(t) + i'_{cap}(t) + i_R = 0$

$$C \frac{dV_o(t)}{dt} + \frac{V_o(t)}{R} = i'(t)$$

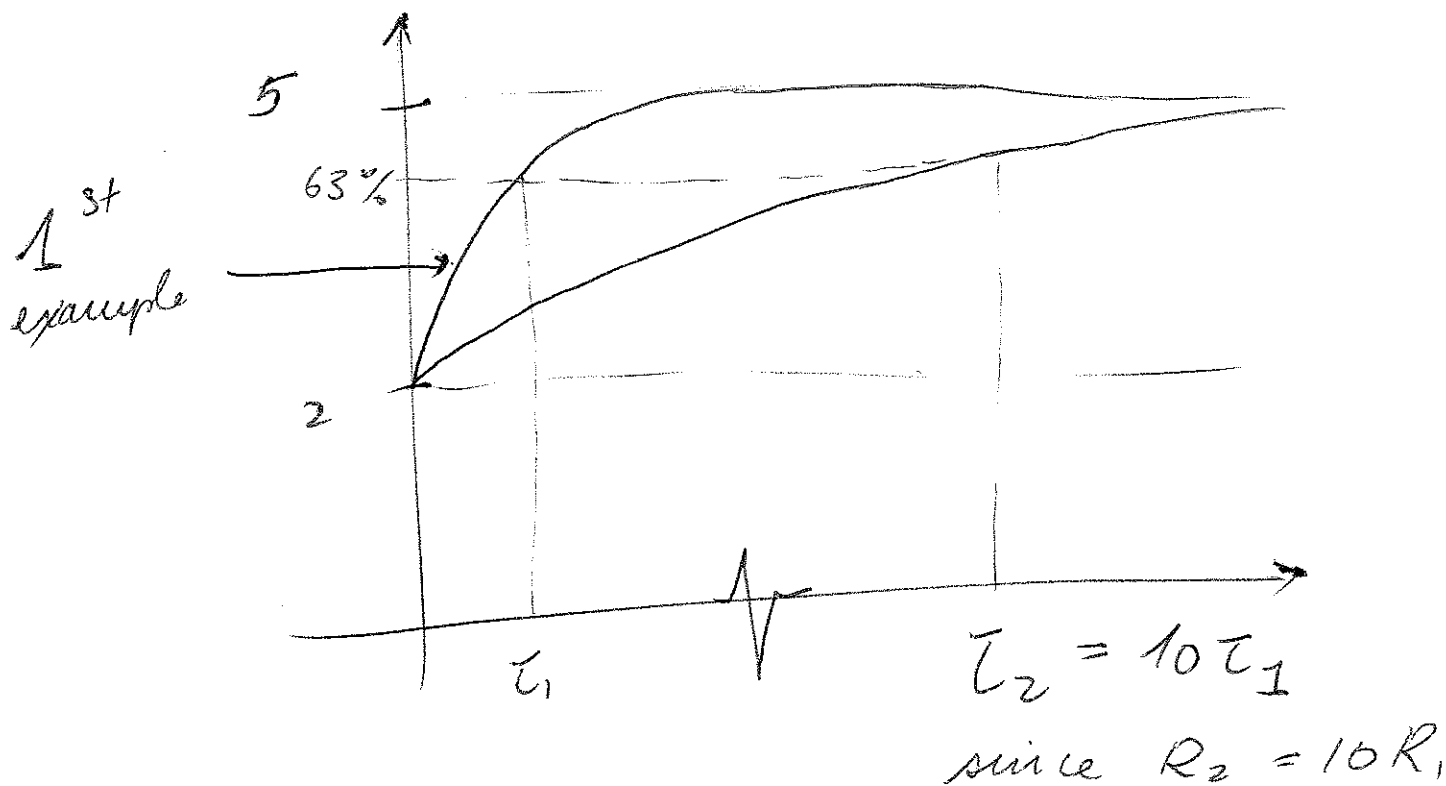
$$\Rightarrow V_o(t) + RC \frac{dV_o(t)}{dt} = \underbrace{R i'(t)}_{v(t) \text{ from previous example}}$$

Note: same equation as when we did a source transformation.

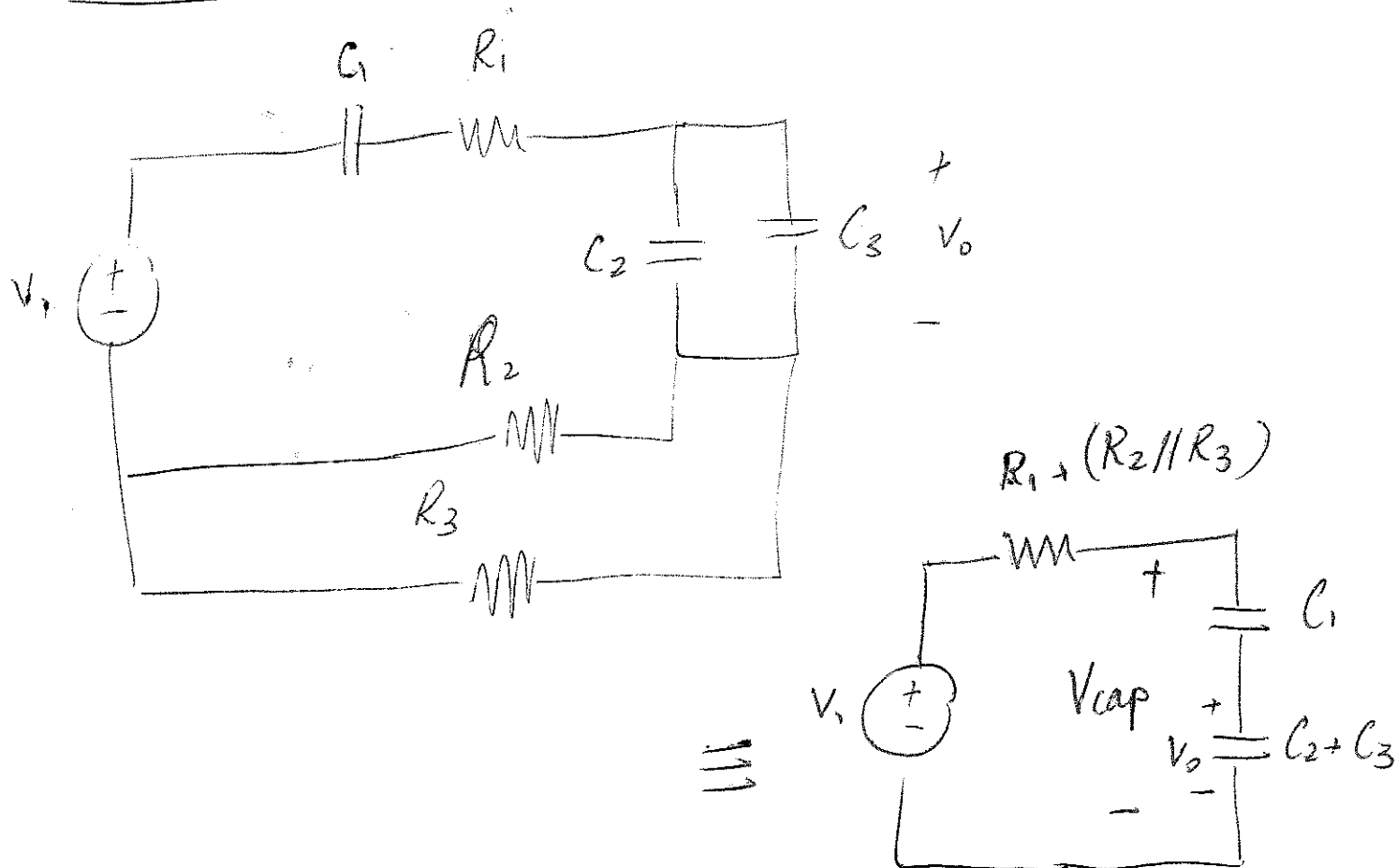
\Rightarrow we know the solution

$$V_o(t) = 5 - 3e^{-t/\tau}$$

but now τ is 10x greater.

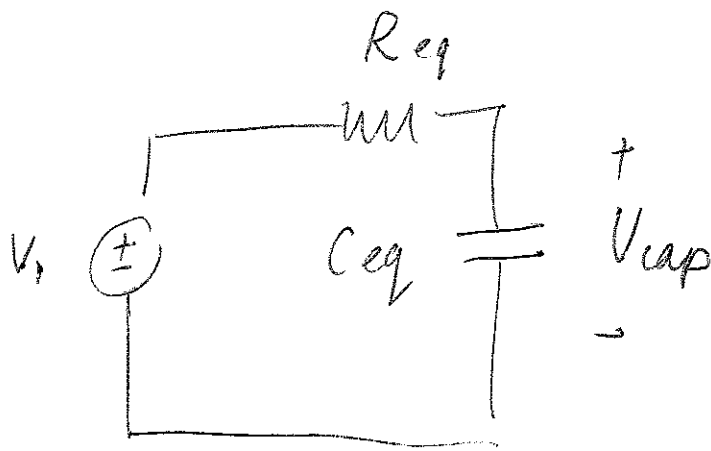


slide 9:



$$V_o = \frac{C_{eq}}{C_2 + C_3} V_{cap}$$

So we can further simplify the CKT:

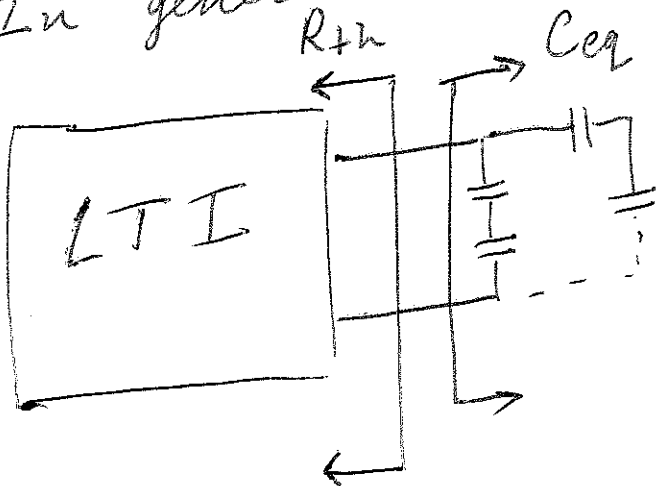


$$V_s = u(t)$$

for $t \geq 0$: $V_{cap}(t) = 1 - 1e^{-t/\tau}$ where $\tau = R_{eq} \cdot C_{eq}$

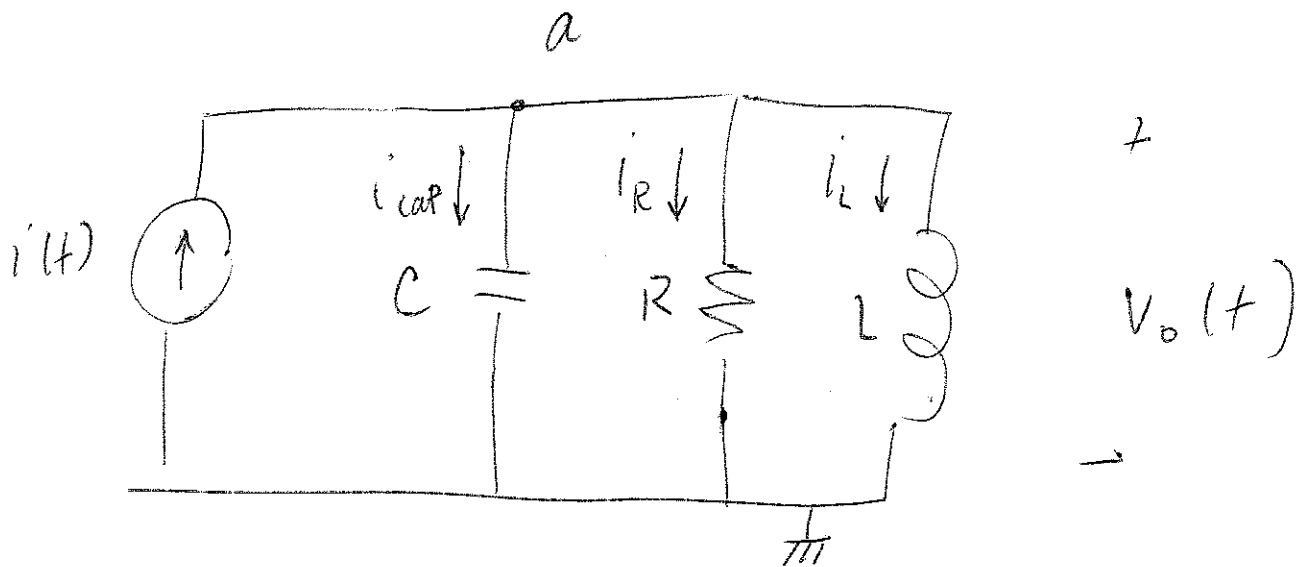
$$\Rightarrow V_o(t) = \frac{C_{eq}}{C_2 + C_3} \left[1 - 1e^{-t/\tau} \right] \text{ for } t \geq 0$$

In general:



$$\tau = R_{th} \cdot C_{eq}$$

Slide 10



RCL @ a:

$$-i(t) + i_{cap} + i_R + i_L = 0$$

$$C \frac{dV_o(t)}{dt} + \frac{V_o(t)}{R} + \frac{1}{L} \int V_o(t) dt + i_L(0) = i(t)$$

$$\frac{d^2 V_o(t)}{dt^2} + \frac{dV_o(t)}{dt} \cdot \frac{1}{RC} + \frac{1}{LC} V_o(t) = \frac{1}{L} \frac{di(t)}{dt}$$

characteristic equation:

$$\frac{d^2 V_o(t)}{dt^2} + \frac{dV_o(t)}{dt} \frac{1}{RC} + \frac{1}{LC} = 0$$

$$\Rightarrow \omega_0 \equiv \frac{d^2 V_o(t)}{dt^2} + \frac{dV_o(t)}{dt} \cdot 2\zeta\omega_0 + \omega_0^2 = 0$$

$$\Rightarrow \omega_0 = \frac{1}{\sqrt{LC}}$$

$$\zeta = \frac{1}{2RC\omega_0} = \frac{1}{2R} \sqrt{\frac{L}{C}}$$

Slide 11: $i'(t) = 1 + u(t) + A \cos(\omega_0 t + \phi)$

split into 2 parts:

$$i'_{\sin}(t) = A \cos(\omega_0 t + \phi)$$

$$i'_{\text{transient}}(t) = 1 + u(t)$$

and solve each one separately. Add
in the end by superposition.

$$a) \quad i(t) = 1 \cdot u(t)$$

$$L = 10 \mu H, \quad C = 1 nF, \quad R = 50 \Omega$$

$\zeta = 1 \Rightarrow$ the solution is of the form:

$$V_o(t) = K_1 + K_2 e^{-st} + K_3 t e^{-st} \quad \text{where}$$

$$s = \omega_0$$

Now use the initial conditions to solve for K_1 , K_2 and K_3 :

$$V_o(0) = 0 \quad \text{because of the cap:}$$

$$K_1 + K_2 = 0$$

$$V_o(\infty) = 0 \quad \text{because of the inductor}$$

$$\Rightarrow K_1 = 0 \quad \Rightarrow K_2 = 0$$

$$i_{cap}(0) = 1$$

since the step current $u(t)$ will all initially flow in the cap. The

$$i_{cap} = C \frac{dV_o(t)}{dt} = C \frac{dK_3 t e^{-st}}{dt}$$

DC 1 A always flows through the inductor and does not cause a transient.

$$i_{cap}(t) = K_3 C \left[e^{-st} + (-s) + e^{-st} \right]$$

$$i_{cap}(0) = K_3 C e^{-s(0)} = K_3 C = 1$$

$$\Rightarrow K_3 = \frac{1}{C}$$

$$\Rightarrow V_0 = \frac{1}{C} + e^{-\omega_0 t}$$

